



C.C. Tatham & Associates Ltd.
Consulting Engineers

BURL'S CREEK EVENT GROUNDS

Township of Oro Medonte

Functional Servicing & Preliminary Stormwater Management Report
Final Report

prepared by:

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prepared for

Burl's Creek Event Grounds
June 2015
(Revised December 10, 2015)

CCTA File 115032-02

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1 Introduction

C. C. Tatham & Associates Ltd. (CCTA) has been retained by Burl's Creek Event Grounds to prepare a Functional Servicing and Preliminary Stormwater Management (SWM) Report in support of pending Official Plan Amendment (OPA) and Zoning Bylaw Amendment (ZBA) applications for their property located in the Township of Oro- Medonte.

1.1 Site Description

The site consists of 228.7 ha of land in the Township of Oro-Medonte. The original Burl's Creek property consists of 41.8 ha of land located east of Line 8 South. Additional lands east and west of the original property have recently been purchased by Burl's Creek. The site is bisected by Burl's Creek which flows in a southerly direction and eventually outlets to Lake Simcoe. The site is bounded by Highway 11 to the north, Line 9 South to the east, Line 7 South to the west, farmer's fields to the south with Line 8 South bisecting the property. Access to the site is provided via numerous field entrances off of Lines 7, 8 and 9 South. The property is legally described as Concession 8, Lot 21 and 22 as well as Concession 9, Lot 22 and 23 (Geographic Township of Medonte) Township of Oro-Medonte.

A Key Plan illustrating the site location is included overleaf.

1.2 Objectives

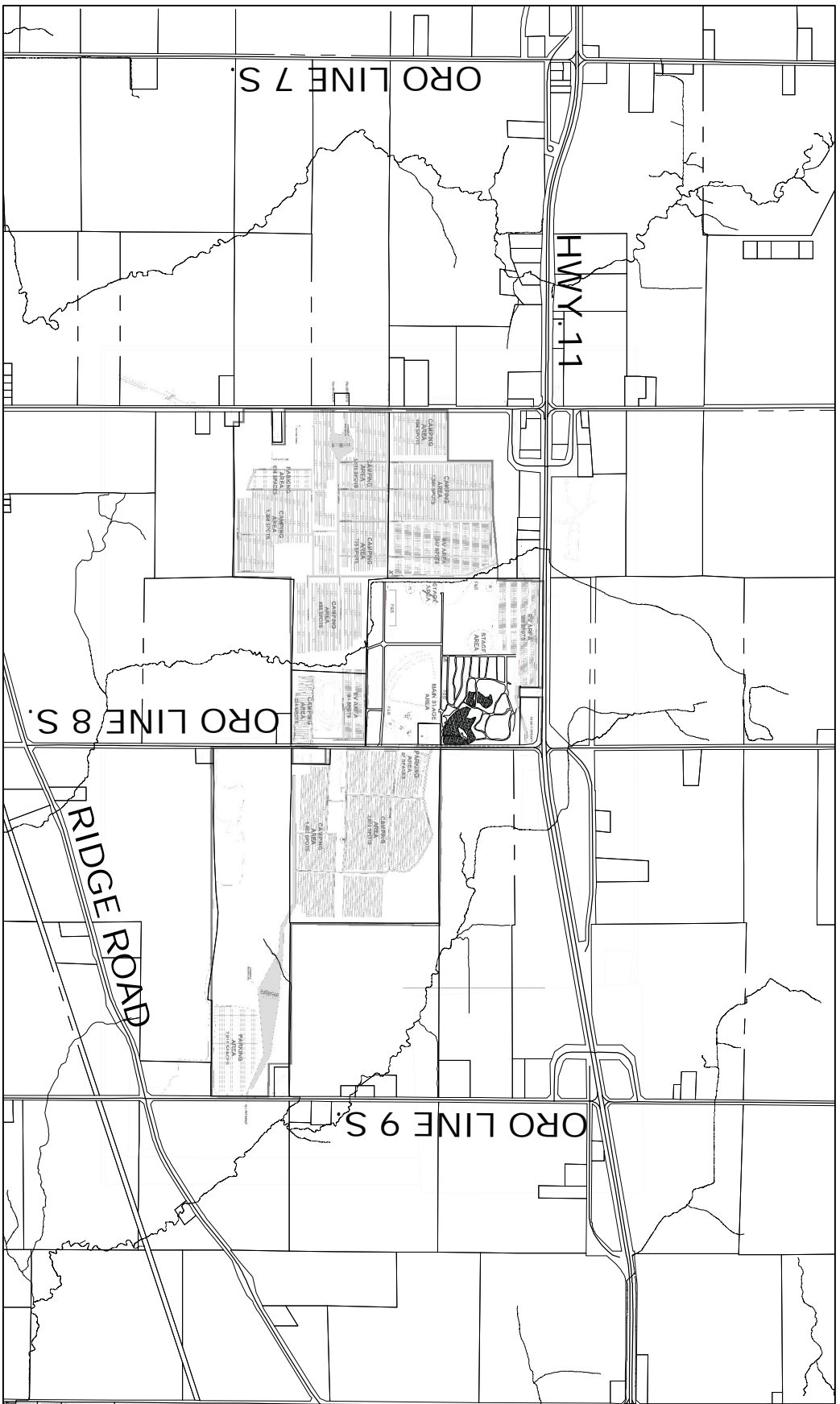
The primary objective of this report is to assess the feasibility of the proposed development with respect to servicing and stormwater management (SWM) and to ensure satisfactory information on these items is presented in support of pending OPA and ZBA applications. This will involve an evaluation of existing and future site conditions. Opportunities and constraints will be evaluated and a preferred SWM plan recommended. The plan will also have regard for the recent grading activity that has been completed on-site and provide recommendations in this regard to ensure compliance with this SWM plan.

1.3 Guidelines & Background Reports

This report was prepared recognizing provincial guidelines on water resources and the environment, including the following publications:

- Ministry of Environment (MOE) Stormwater Management Practices Planning and Design Manual (2003);
- Ministry of Natural Resources (MNR) Natural Hazards Training Manual: Provincial Policy Statement, Public Health and Safety Policies 3.1 (1997);

- Lake Simcoe Regional Conservation Authority (LSRCA) Technical Guidelines for Stormwater Management Submissions (April 26, 2013); and
- MOE Lake Simcoe Protection Plan (LSPP) (2009).



C.C. Tatham & Associates Ltd.
 Consulting Engineers
 Collingwood Brantford Oshawa Barrie

BURL'S CREEK EVENT GROUNDS

KEY PLAN

SCALE: NTS

DATE: MAY 2015

DWG. No. FIG-1

2 Existing Drainage Conditions

2.1 Background Information

Information regarding the existing topography, ground cover and drainage patterns was obtained through a review of relevant background studies, available plans and base mapping and was confirmed with topographic survey of selected features and field review.

2.2 Existing Conditions

Topographic information obtained indicates that part of the site slopes gently towards Burl's Creek, which traverses the site. The remaining site area slopes towards Allingham Creek located east of the site. Catchment 101 accounts for the majority of the site between Line 7 and 8 South and drains directly into Burl's Creek which bisects the catchment. A small portion of area south of Catchment 101 (Catchment 104) drains overland as sheet flow onto the neighbouring property and ultimately into a tributary to Burl's Creek and then to Burl's Creek just upstream of Line 8 South. Along the west edge of the property, Line 7 South has minor roadside ditches that collect stormwater from the road and convey it south towards Lake Simcoe. The subject property contributes little to no drainage to the Line 7 South roadside ditch.

The northeast corner of the site, west of Line 8 South (Catchment 106), drains east to a system of on-site ponds that collects water and outlets intermittently to the Line 8 roadside ditch. We note that these ponds have been identified by LSRCA as a wetland. The ditch then flows west under Line 8 South through a 1.25 m x 1.65 m corrugated steel pipe arch culvert. Runoff from Catchment 106 combines with Catchment 102 east of Line 8 where it drains overland towards Allingham Creek. The remaining portion of the site between Line 8 and 9 South (Catchments 103 and 105) flow overland towards the Line 9 roadside ditch, through a cross culvert across Line 9 South and then to Allingham Creek. Drainage from Line 8 is collected in roadside ditches with the northern portion draining north towards the Line 8 wetland outlet location and then to Allingham Creek and the southern portion draining south and discharging to Burl's Creek. The subject site does not contribute drainage to the Highway 11 drainage system. Existing drainage patterns as described above are depicted on the appended Drawing ODP-1.

215.27 ha of external drainage from north of Highway 11 (Catchment 301) flows into Burl's Creek and is conveyed under Highway 11 through a culvert and through the subject site.

Soil mapping shows the site soils to be predominantly Vasey sandy loam, which is characterized by good drainage. Smaller areas of Sargeant gravelly sand loam, which has excellent drainage properties, are also present. The area of the existing ponds is identified as Allston sandy loam.

Table 1: Summary of Existing Condition Peak Flow Rates

Storm Event	Peak Flow to Burl's Creek Outlet A (m ³ /s)		Peak Flow from to Allingham Creek Outlet B (m ³ /s)	
	SCS	CHI	SCS	CHI
2-year	1.05	0.76	0.47	0.36
5-year	1.85	1.43	0.83	0.67
10-year	2.46	1.93	1.12	0.91
25-year	3.32	2.65	1.51	1.27
50-year	4.01	3.28	1.83	1.58
100-year	4.74	3.91	2.18	1.89
Timmins	-	11.80	-	4.40

3 Recent Grading

3.1 Overall Site Grading

The goal of the site alteration work that was recently carried out was to create a workable event space while limiting disturbance as much as possible. Mass grading operations were avoided and minor regrading was carried out only as required to even out grassed surfaces to serve as camping and parking areas. Gravel driveways and laneways were generally constructed at grade. As a result, existing drainage patterns will generally be maintained.

Additional site grading is proposed only for the purpose of constructing the proposed stormwater management facilities. A preliminary Site Grading Plan (Drawing SG-1) is appended to show the overall grading plan and general drainage patterns.

3.2 Site Grading Adjacent to MTO Lands

A berm was constructed adjacent to Highway 11, between Line 7 and Line 8 South. This berm represents the only site alteration with the potential to impact the Highway 11 drainage system, as it could direct a small amount of drainage (originating from the berm itself) to the Highway 11 ditch. While the quantity of runoff that could be directed to Highway 11 is very small, we nonetheless have designed a cutoff swale to intercept runoff from the berm and direct it easterly and then south to the on-site wetland. The details of this swale are shown on the attached Drawing MTO-1.

4 Servicing

4.1 Water Supply & Sanitary Sewage Disposal

The provision of on-site water treatment is not proposed at this time. For larger scale events, potable water will be trucked to the site to meet event demands. A qualified contractor will be selected to provide the required potable water service for the larger events. Between 70 and 80 large plastic storage tanks will be located throughout the site to store the water during these events. Tanker trucks will replenish the water supply as needed prior to and during the events. The City of Barrie Water Supply Department has agreed to provide the water supply and a hydrant located approximately 10 minutes from the site has been identified as the supply location.

Sanitary servicing requirements for larger events will be met using portable washroom facilities. A qualified contractor will be selected to provide the portable washroom facilities for these events. Approximately 700 portable toilets will be provided throughout the site during larger events. These units will be pumped as required and sanitary waste hauled off-site throughout the events as required. The Orillia Waste Water Treatment Centre will serve as the disposal location for the hauled sanitary waste and has agreed to provide 24 hour access to their facility for the duration of these events. The washroom units will be trucked in and out of the site as required.

4.2 Roadways & Transportation

A transportation review has been completed by CCTA to investigate impacts from the proposed development on surrounding roads.

The Traffic Impact Study, dated June 12, 2015, identifies that access to the event grounds will be provided from Line 7, 8 and 9 South. No access to Highway 11 is proposed.

4.3 Utilities

A qualified contractor will be selected to provide the electrical servicing required for the larger scale events. The RV campsites will be powered by silent generators. Each generator will have the necessary distribution panels, waterproof receptacles and cabling.

5 Future Drainage Conditions

5.1 Design Criteria

Criteria to be met with respect to water quantity and water quality control related to the development of the site are summarized as follows:

- the site will be developed in accordance with Township of Oro-Medonte Standards;
- provide “Enhanced” level water quality control, to ensure the development will have no negative impacts on the water quality of downstream watercourses;
- ensure post-development runoff rates will not increase from pre-development rates for storms up to and including the 1:100 year event, while maintaining current flow rates beyond the property boundary;
- address safe conveyance of storm flows from the Regional (Timmins) Storm event; and
- per LSPP Designated Policy 6.26, for site alteration that occurs within 120 m of a key hydrologic feature (which includes all permanent watercourses) it should be demonstrated that the alteration will result in no adverse effects on the hydrologic function of the feature

We note that the Township of Oro-Medonte’s Comprehensive Stormwater Management Master Plan, which has recently been finalized, offers no specific recommendations for development in the Burl’s Creek and Allingham Creek watersheds, as they do not contain settlement areas, however the general recommendations of that document with regard to stormwater management will be referenced and adhered to.

5.2 Proposed Development

The development includes an expansion to the existing Burl’s Creek Event Grounds. As referenced in Section 3, site alteration has taken place and includes the creation of additional gravel driveways and pedestrian paths, gravel pads for temporary stages, minor grading works as required to even out grassed camping/parking areas. No new permanent structures have been constructed. Limited areas of the site have had tile drains installed to allow for improved drainage from low lying/flatter sloped areas without mass grading operations. The total gravel/impervious cover for the site, after the recent site alterations is approximately 10%. Asphalt surfaces are not proposed and would not be desirable given the intended use of the property. We note that the area of new gravel surface was approximated using a site plan provided by Burl’s Creek and we recommend that the actual gravel surface be confirmed in the field at the detailed design stage. This will allow the required water quantity and quality storage volumes to be refined to more accurately reflect the extent of site alterations undertaken.

Existing drainage patterns will generally be maintained, with the site continuing to drain towards the existing site outlets (Burl's Creek or Allingham Creek). At present, flows from the site are higher than under existing conditions. Through the provision of appropriate SWM controls, peak flow rates will be maintained at existing rates for all site outlets.

Catchment 204 has a slight decrease in drainage area from the existing condition due to the minor grading alterations directing flow into the conveyance swales and ultimately Burl's Creek. Catchments 202 and 205 experienced no site alteration and are therefore identical to the existing Catchments 102 and 105. The proposed drainage patterns are shown on Drawing ODP-2.

6 Proposed SWM Plan

An understanding of specific issues, constraints and opportunities pertaining to the site was gained through an analysis of relevant background information. A number of quality and quantity control measures are available and are identified here for consideration. Opportunities for maximizing the effective use of the control measures are discussed in this section.

6.1 Source/Conveyance Controls

Potential source control measures include directing pervious or gravel surfaces to vegetated buffer strips or soakaway pits. These measures provide both quality and quantity benefits, including infiltration enhancement and peak flow reduction, as well as pollutant removal.

Conveyance controls include low-sloped grass swales and pervious pipe systems. These systems can be very effective for reducing runoff volumes, increasing groundwater recharge and improving water quality.

The native soils on the subject site are sandy loam and gravelly sandy loam, which are conducive to the use of infiltration practices.

6.2 End of Pipe Controls

Potential end-of-pipe facilities include extended detention wet ponds, dry ponds, constructed wetlands, oil/grit separators, filter strips and infiltration basins. An end of pipe facility is effective for meeting water quantity and water quality requirements for large catchment areas.

6.3 Preferred SWM Strategy

As indicated above, SWM controls could be provided by a number of feasible alternatives. These include: grassed swales, infiltration trenches, dry ponds and extended detention ponds. The SWM strategy can rely primarily on one type of practice, or utilize a combination of practices.

For the purpose of confirming the feasibility of this approach, we have assumed that conveyance controls will be implemented and undertaken a conceptual design of this system. This system would consist of a series of enhanced swales located along the gravel driveways and pedestrian pathways. The swales would be low profile (typically 0.5 m depth, with 3:1 side slopes) to ensure they do not represent a hazard. The swales would provide both water quantity and water quality control. Water quality would be provided through infiltration and filtration, while water quantity control would be provided by attenuating runoff behind rock check dams and culvert controls.

The OTTHYMO hydrologic model was used to determine peak flow rates from the subject site under existing and proposed conditions for both the 4-hour Chicago (CHI) and 24-hour SCS storm distributions. The model was then used to determine the required water quantity storage volume to attenuate the post-development peak flow during the 100-year storm to pre-development levels. Model results for the pre and post-development scenarios, along with hydrologic input parameters, have been included in **Appendix A** and **Appendix B** respectively.

Table 2: Summary of 100-year Peak Flow Rates

	Outlet Location (Catchment Number)								
	Outlet A+B (102+106/ 202+206)	Outlet C (103/203)	Outlet D (105/205)	Outlet E (101/201)	Outlet F (104/204)	Outlet E+F Total Flow to Burl's Creek (Node 301)	Outlet A+B+C+D Total Flow to Allingham Creek (Node 306)	Burl's Creek Flow at Lake Simcoe	Allingham Creek Flow at Lake Simcoe
Existing 100-yr SCS (m ³ /s)	1.46	0.61	0.21	2.33	0.93	4.74	2.18	10.71	10.77
Proposed 100-yr SCS (m ³ /s)	1.46	0.61	0.21	1.73	0.93	4.27	1.87	10.14	11.36
Existing 100-yr CHI (m ³ /s)	1.34	0.450	0.17	2.04	0.82	3.91	1.89	8.72	8.68
Proposed 100-yr CHI (m ³ /s)	1.27	0.49	0.17	1.51	0.82	3.52	1.87	8.33	9.25
Quantity Control Storage Volume Required (m ³)	3850	1822	0	0	460	-	-	-	-
Quality Control Volume Required (m ³)	520	750	0	1116	575				

The results shown in the Table above confirm that the post-development peak flow rates at the site outlet can be maintained at pre-development levels when SWM controls are provided. The hydrologic impact of the subject site and the proposed SWM controls was also assessed in the subwatershed context, with pre and post-development flow rates from Burl's Creek and Allingham Creek to Lake Simcoe being calculated. The results show that development will not adversely impact flow rates from Burl's Creek to Lake Simcoe. Small increases in flow rates to Lake Simcoe from Allingham Creek are shown to result from the site development. This increase is due to a change in the timing of flow releasing from the site and how it combines with upstream and downstream flows. The changes are deemed very minor and do not account for the potential attenuation effect of the on-site ponds. At the detailed design stage, additional modelling will be completed to account for the attenuation effect from the on-site ponds. It is expected that the results of the analysis with the on-site ponds and wetlands included will show that the timing of the peak flow from the site under pre-development conditions is similar to that under post-development conditions and the small difference in peak flow rates at Lake Simcoe will no longer appear in the model. Additional commentary with regard to peak flows and potential downstream impacts are included in Section 6.4.

The required water quantity storage volume of the conceptual SWM system, which is the volume required to control post-development 100-year storm to pre-development levels, is 460 m³ for flow to Burl's Creek and 5,672 m³ for flow to Allingham Creek. Water quality storage requirements for the system were determined based on the MOE SWM Manual criteria for Enhanced Level water quality control. Each catchment was considered individually when determining the required water quality storage volume. The proposed "impervious" surface for each catchment, which in this case is gravel, and the contributing drainage areas were used in determining the water quality volume requirement. This level of impervious cover corresponds to an infiltration storage volume requirement of between 15.5 and 17.7 m³/ha depending on the catchment. The required water quality storage volumes are provided in Table 2 and supporting calculations can be found in **Appendix C**.

The drawdown time for runoff stored in the swales behind the check dams was calculated to be approximately 15 hours based on the conceptual design. This calculation confirms that the proposed infiltration storage volume would not result in ponding for a significant period of time, and that storage volume will quickly become available for successive runoff events.

A conceptual swale system, with a total length of 7,130 m and resulting storage volume of 8,021 m³, based on a typical swale cross-section, was sized and is as shown on Drawing SG-1. For each catchment area, the greater of the calculated water quantity or quality volume was used to determine the required swale length. The total storage volume provided exceeds the required storage volume of 7,363 m³, thus confirming the feasibility of providing the required SWM controls on-site. Preliminary design calculations are provided in **Appendix C**.

6.4 Impact on Hydrologic Function of Burl's Creek and Allingham Creek

Much of the additional property acquired by Burl's Creek was previously active agricultural land that was used for a combination of row crop and pasture. Review of aerial imagery over the last 10 years indicates that approximately 72 ha of this agricultural land was row crop.

The modeling completed has confirmed that under the proposed land use, this 72 ha will actually see a decrease in runoff, even with the addition of some gravel laneways, as the entire area will be grassed. The recently installed tile drains were also considered in the hydrologic model as providing a more efficient drainage pattern for certain areas. Based on these results it is our opinion that the impact of recently installed tile drainage in the selected areas shown on the attached drawing prepared by Burl's Creek, titled "Burl's Creek - Drainage", will be compensated for by this change in land cover.

The proposed SWM plan relies on infiltration controls and will serve to maintain the natural water balance as much as possible. It is therefore our assessment that, with the recommended SWM controls, the hydrologic function of Burl's Creek and Allingham Creek will not be adversely impacted by the site alteration.

7 Siltation & Erosion Plan

Siltation and erosion controls will be implemented for all future construction activities, including topsoil stripping, material stockpiling, swale construction and grading operations. A detailed erosion and sediment control plan for the site will be prepared with the final design and will include the following:

- all erosion control measures will be specified in accordance with Township of Oro-Medonte standards;
- silt fences will be erected before commencement of any grading operations to control sediment movement;
- outlet locations for storm drainage will be protected with appropriate permanent erosion control measures, including level spreaders where discharge will drain overland and rip-rap or other protective surfaces for watercourse outlets; and
- regular inspection of control measures will be instituted and repairs will be made as necessary.

Long term siltation and erosion control will be enhanced with a revegetation strategy for disturbed areas.

8 Conclusion & Recommendations

The work completed for this report has confirmed that the SWM requirements for this site can be met through the implementation of the SWM measures proposed. The plan in place supports the pending Official Plan Amendment and Zoning Bylaw Amendment applications.

Site alteration has recently occurred and consists of minor grading of grassed parking/camping spaces, gravel driveways and pedestrian paths. Existing drainage patterns have been generally maintained, with stormwater continuing to be directed overland towards Burl's Creek and Allingham Creek.

Stormwater management quantity and quality controls can be provided through application of a number of SWM alternatives. For the purpose of confirming the feasibility of providing the required on-site SWM controls, conceptual design of a system of grassed swales was carried out. The grassed swales would manage runoff and allow a portion of runoff to infiltrate and provide controlled release for the remainder.

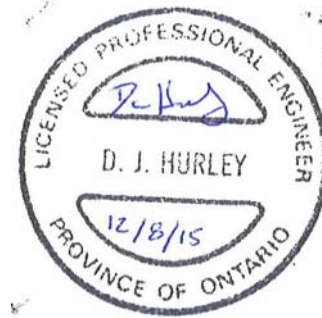
Permanent services are not currently proposed for the development. Servicing needs will be met through temporary servicing options. Potable water will be trucked onto the site and portable washrooms facilities will be brought in and out as needed.

Siltation and erosion control will be provided with the proper construction mitigation efforts. Long-term erosion control will be enhanced with an effective revegetation strategy.

Detailed design of the specific SWM facilities, as required, will be provided at the final design stage, which will occur in conjunction with a Site Plan Application, following approval of the OPA and ZBA. The detailed design should include field confirmation of the extent of gravel surfaces added to refine the water quantity and water quality storage volumes. The work completed to date confirms the feasibility of providing appropriate site servicing and stormwater management for the subject site.

A Kellett

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Project Manager

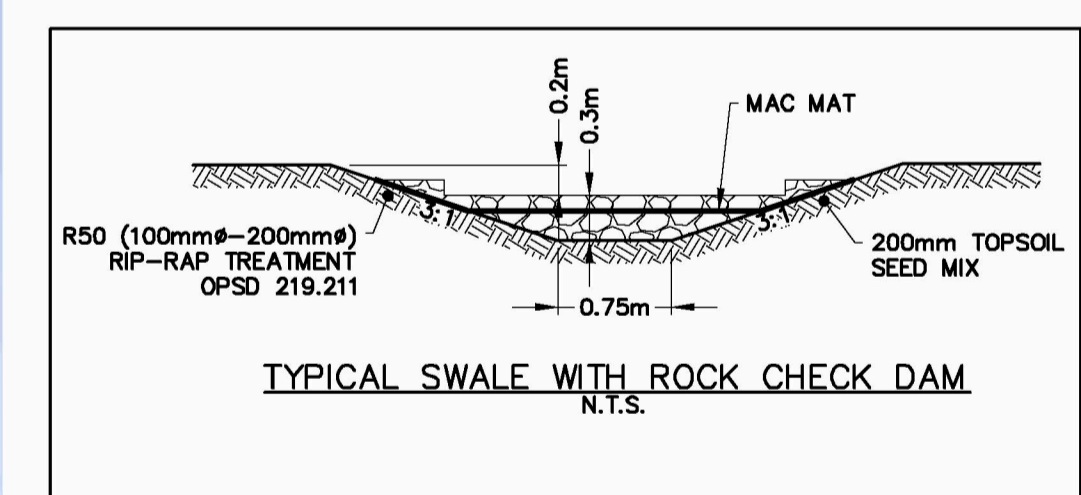
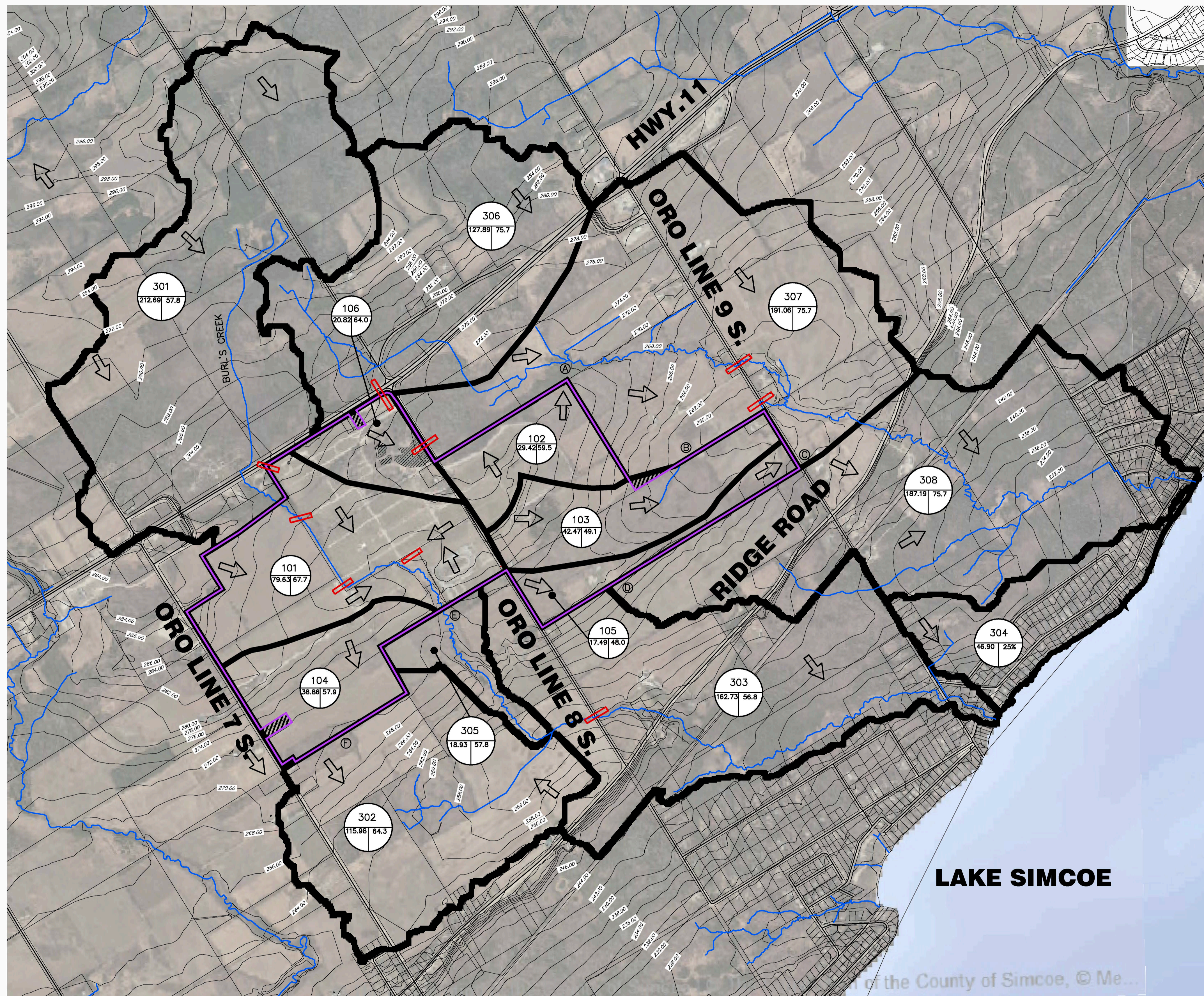
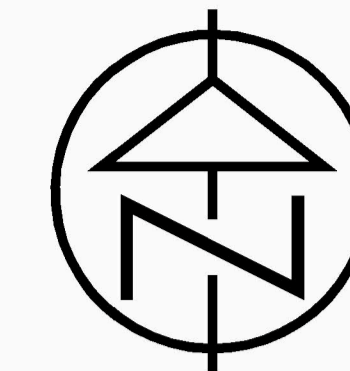


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- LEGEND**
- OUTLET LOCATION
 - EXISTING CULVERT
 - PROPERTY LINE
 - DRAINAGE BOUNDARY
 - PROPERTY NOT OWNED BY BURL'S CREEK
 - OVERLAND FLOW ROUTE
 - DRAINAGE AREA LABEL
 - CURVE NUMBER/% IMPERVIOUS
 - AREA (ha)

LEGEND

CONTRACT DRAWINGS
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NO.	REVISIONS	DATE	INITIAL

APPROVED

BURL'S CREEK EVENT GROUNDS
180 8TH LINE SOUTH, ORO MEDONTE, ON L0L2X0

OVERALL DRAINAGE PLAN

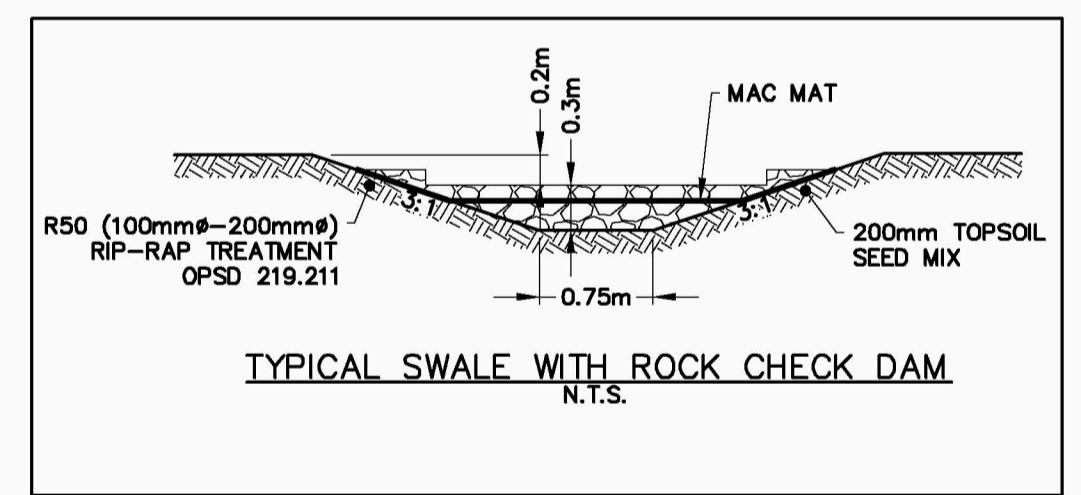
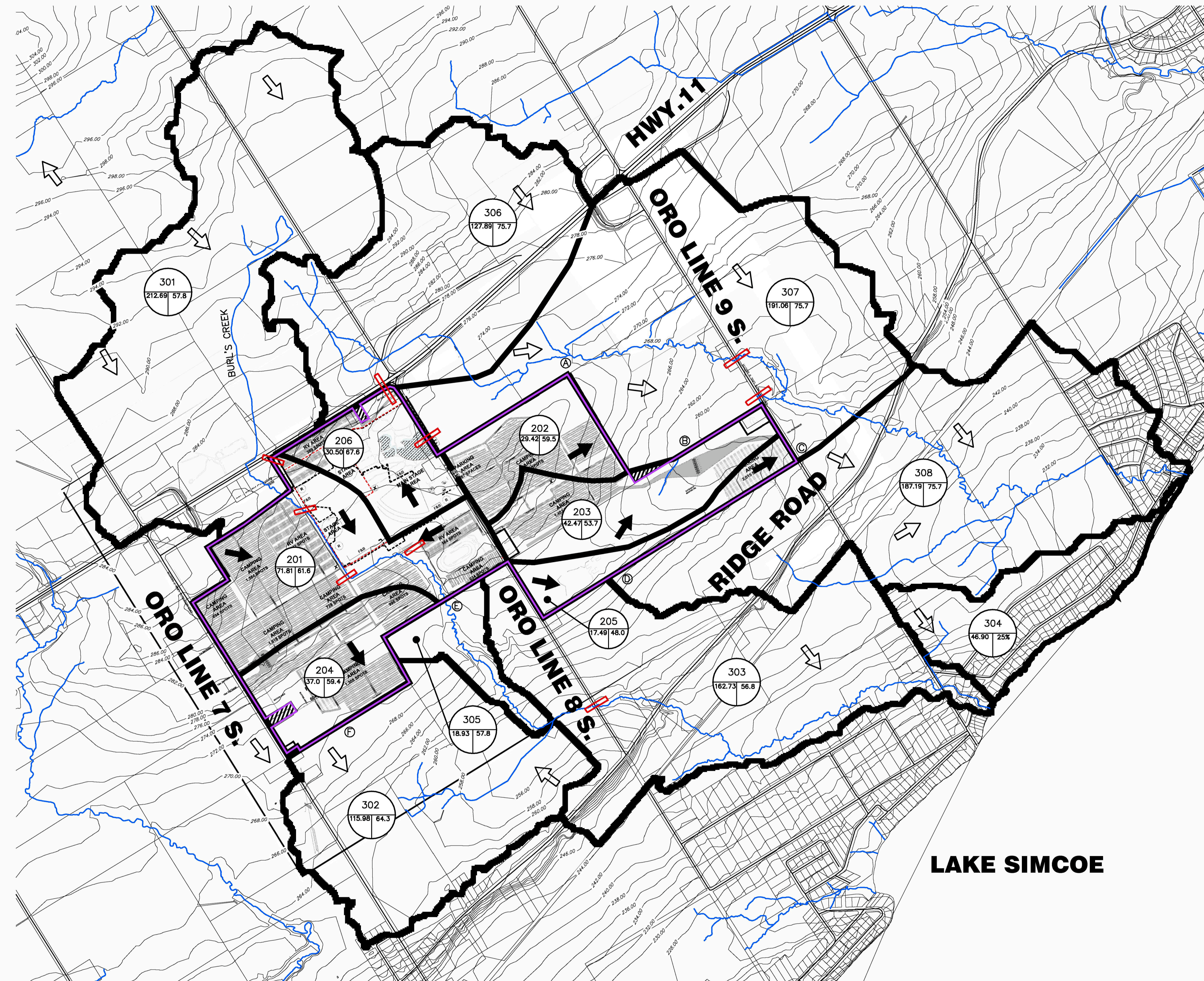
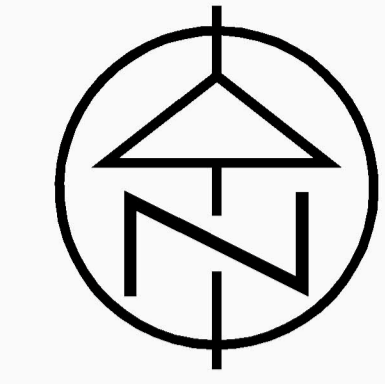
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Collingwood Bracebridge Orillia Barrie

SCALE: 1:500

DESIGN: AR CHECKED: AK JOB NO. 115032

DRAWN: SD DATE: MAY/2015 DWG. **ODP-1**



- LEGEND**
- OUTLET LOCATION
 - EXISTING CULVERT
 - PROPERTY LINE
 - DRAINAGE BOUNDARY
 - PROPERTY NOT OWNED BY BURL'S CREEK
 - POST-CONSTRUCTION OVERLAND FLOW ROUTE
 - EXISTING OVERLAND FLOW ROUTE
 - DRAINAGE AREA LABEL
 - CURVE NUMBER
 - AREA (ha)

LAKE SIMCOE

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BURL'S CREEK EVENT GROUNDS
180 8TH LINE SOUTH, ORO MEDONTE, ON L0L2X0

OVERALL POST-DEVELOPMENT DRAINAGE PLAN

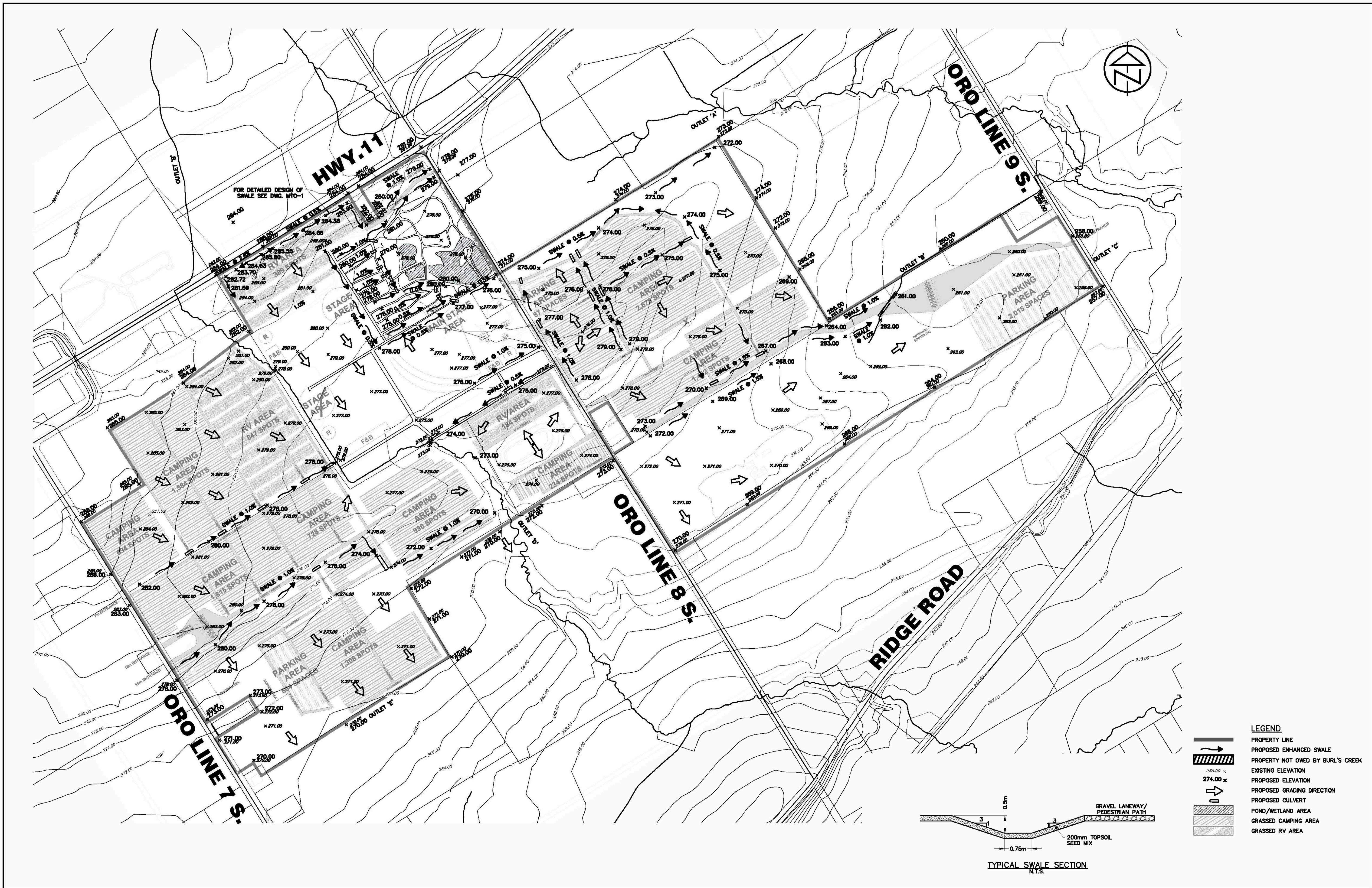
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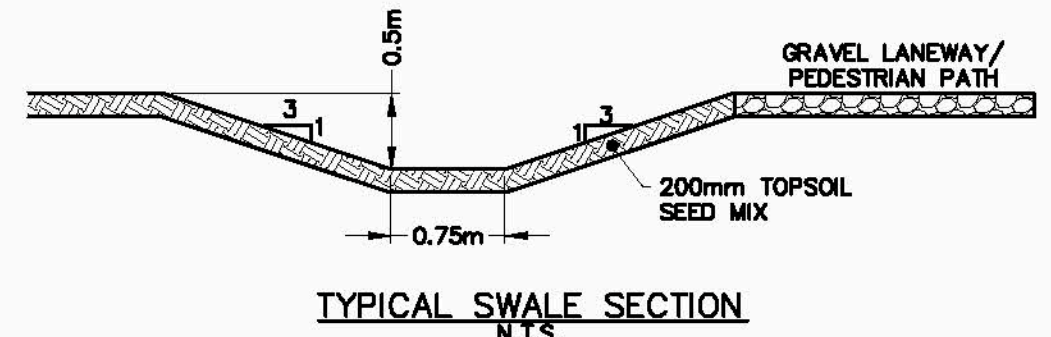
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DESIGN: AR CHECKED: AK JOB NO. 115032

DRAWN: SD DATE: MAY/2015 DWG. **ODP-2**



- LEGEND**
- PROPERTY LINE
 - PROPOSED ENHANCED SWALE
 - PROPERTY NOT OWNED BY BURL'S CREEK
 - EXISTING ELEVATION
 - PROPOSED ELEVATION
 - PROPOSED GRADING DIRECTION
 - PROPOSED CULVERT
 - POND/WETLAND AREA
 - GRASSED CAMPING AREA
 - GRASSED RV AREA



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NO.	REVISIONS	DATE	INITIAL

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BURL'S CREEK EVENT GROUNDS
 180 8TH LINE SOUTH, ORO MEDONTE, ON L0L2X0

OVERALL GRADING PLAN

C.C. Tatham & Associates Ltd.
 Consulting Engineers

Collingwood Bracebridge Orillia Barrie

SCALE: 1:5000
 DESIGN: AR CHECKED: AK
 DRAWN: SD DATE: MAY/2015

JOB NO. 115032
 DWG. **SG-1**

LEGEND

PROPERTY LINE

PROPOSED ENHANCED SWALE

PROPERTY NOT OWNED BY BURL'S CREEK

EXISTING ELEVATION

PROPOSED ELEVATION

PROPOSED GRADING DIRECTION

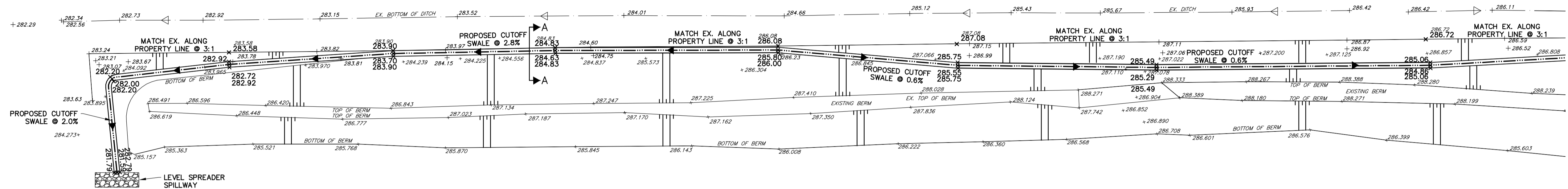
PROPOSED CULVERT

POND/WETLAND AREA

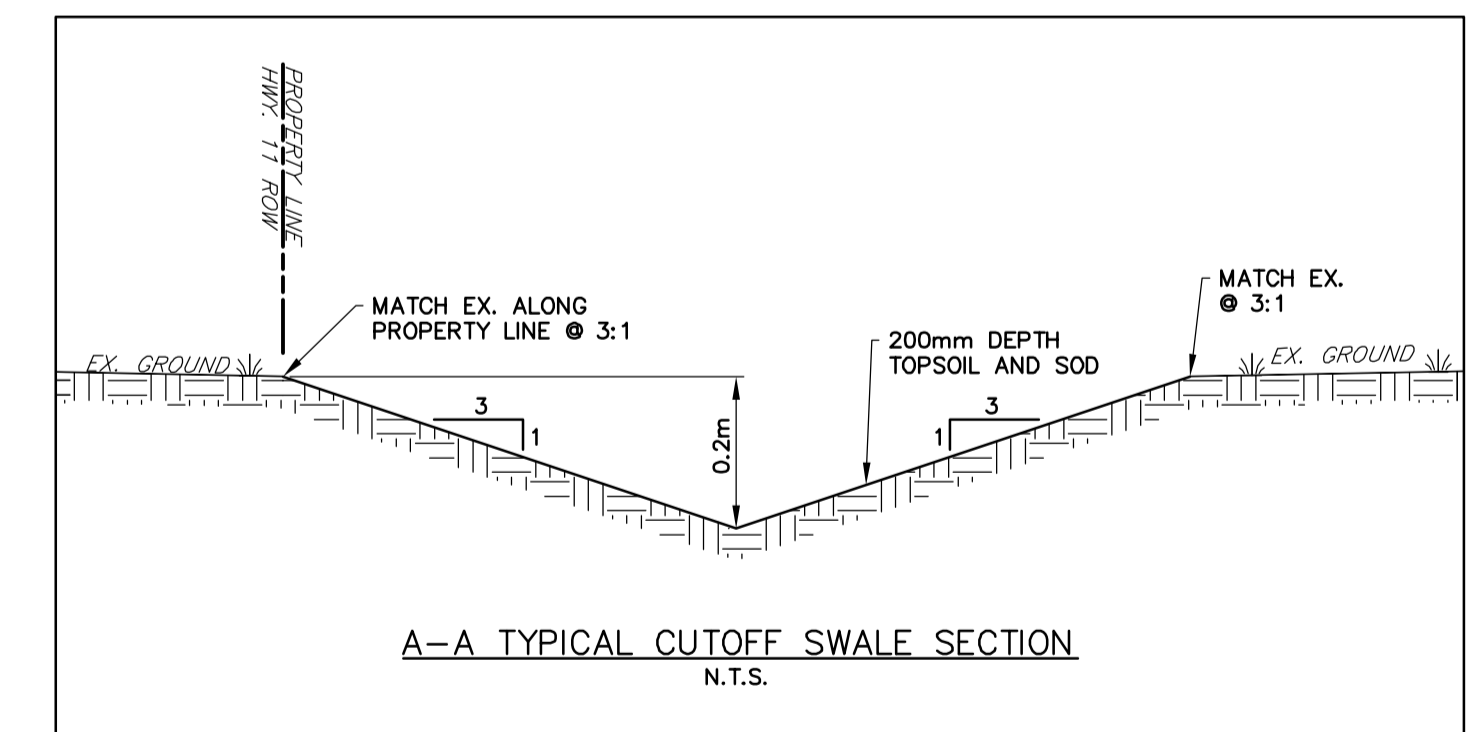
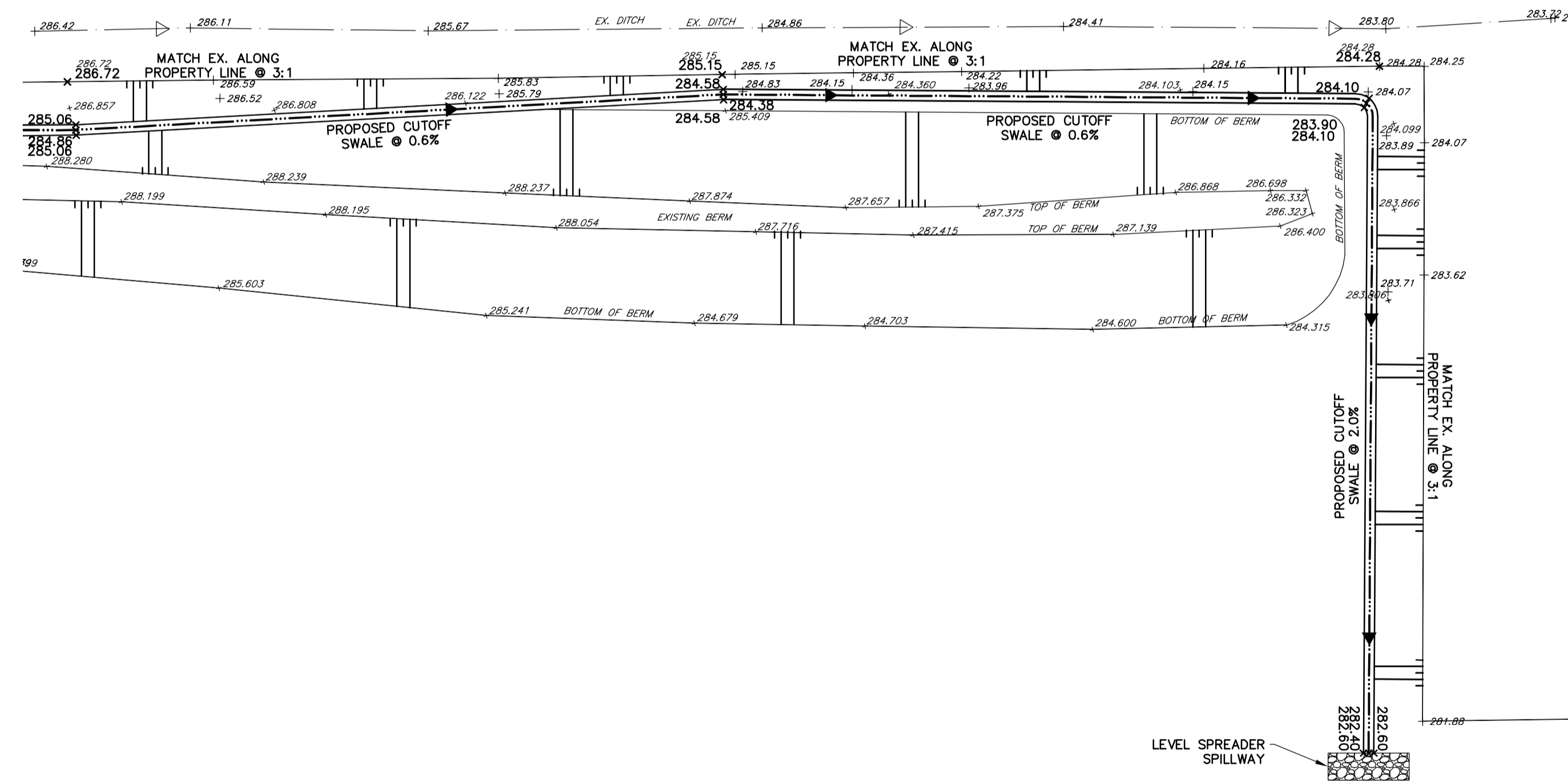
GRASSED CAMPING AREA

GRASSED RV AREA

HWY. 11



HWY. 11



LEGEND

CONTRACT DRAWINGS
 CONTRACTOR MUST VERIFY ALL DIMENSIONS AND BE RESPONSIBLE FOR SAME. ANY DISCREPANCIES MUST BE REPORTED TO THE ENGINEER BEFORE COMMENCING WORK. DRAWINGS ARE NOT TO BE SCALED.
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NO.	REVISIONS	DATE	INITIAL

APPROVED

BURL'S CREEK EVENT GROUNDS
 180 8TH LINE SOUTH, ORO MEDONTE, ON
 LOL2X0

CUTOFF SWALE ADJACENT
 TO MTO ROW



C.C. Tatham & Associates Ltd.
 Consulting Engineers

Collingwood Bracebridge Orillia Barrie

SCALE: 1:500

DESIGN: AR

DRAWN: SD

CHECKED: AK

DATE: MAY/2015

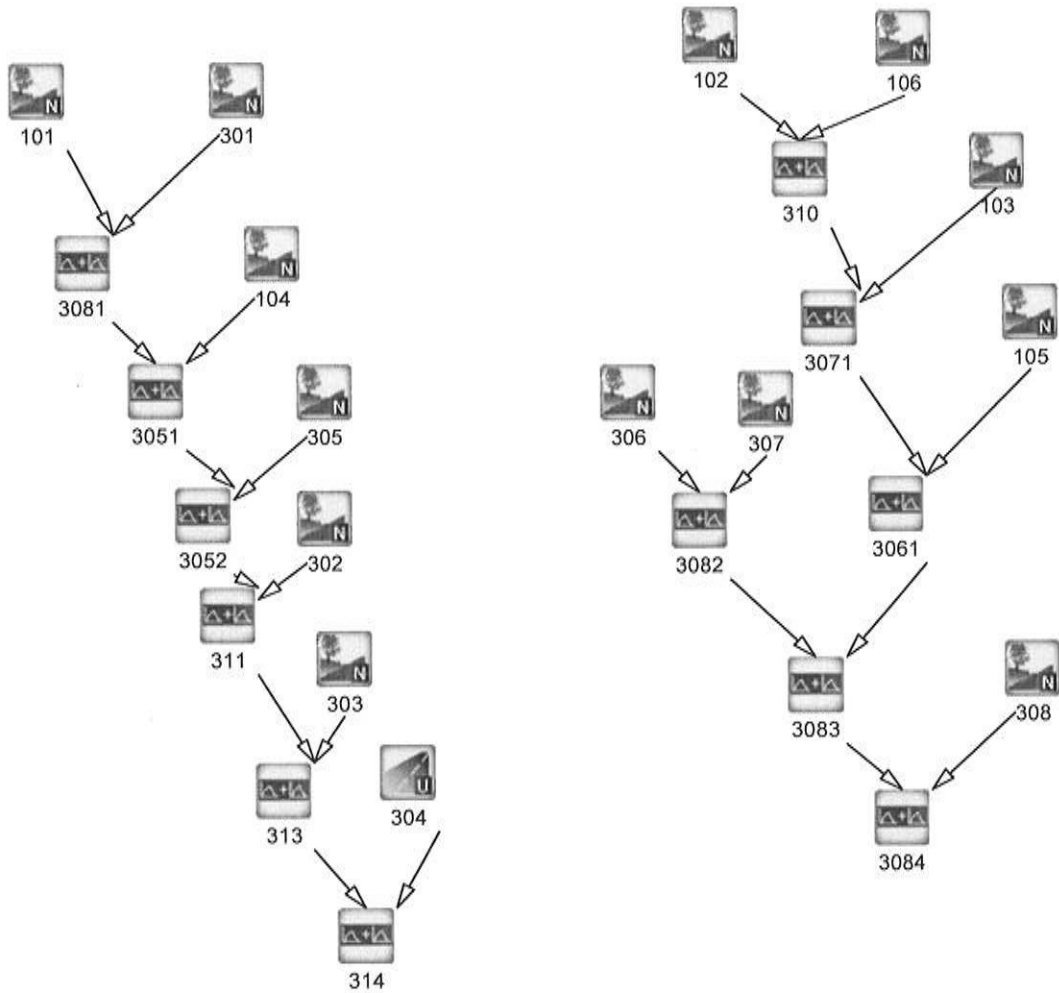
DWG.

JOB NO. 115032

MTO-1

**APPENDIX A:
PRE-DEVELOPMENT HYDROLOGY CALCULATIONS**

Existing Conditions OTTHYMO Model Schematic





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Collingwood Bracebridge Orillia Barrie

Project:	Burls Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

Burls Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																							
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Cultivated		Gravel		Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	
gus	GUERIN	AB	Sand Loam	1	79.63	1	4.778	0.06	46	0	59	71.67	0.9	68	1.593	0.02	89	1.593	0.02	100	0	50	67.74
stsl	SARGENT	AB	Sand Loam	1	0		0		46	0	59	0		68	0	89	0	100	0	0	0	50	0
vasl	VASEY	AB	Sand Loam	1	0		0		46	0	59	0		68	0	89	0	100	0	0	0	50	0
ans	ALLISTON	AB	Sand Loam	1	0		0		46	0	59	0		68	0	89	0	100	0	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0	#N/A	0		#N/A	0	#N/A	0	#N/A	0	0	0	#N/A	0
Totals					79.63	1	4.778	0.06		0	0	71.67	0.9	68	1.593	0.02	89	1.593	0.02	100	0	50	67.7

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

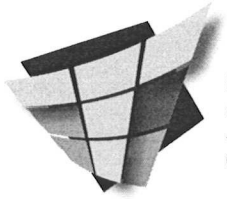
Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction mm

Wetlands	12
Woods	10
Cultivated	7
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Cultivated	0.22	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.234	#N/A	#N/A	#N/A	#N/A



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Checked By:	ALK
Subject:	CN Calculator

BurIs Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows		Gravel			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type	
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN				
gus	GUERIN	AB	Sand Loam	1	29.42	1	3.825	0.13	46	23.54	0.8	59	0	51	1.765	0.06	89	0.294	0.01	100	0	0	50	59.52	
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	51	0	0	89	0	0	100	0	0	50	0	
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	51	0	0	89	0	0	100	0	0	50	0	
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	51	0	0	89	0	0	100	0	0	50	0	
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	
Totals					29.42	1	3.8246	0.13	46	23.536	0.8	59	0	51	1.7652	0.06	89	0.2942	0.01	100	0	0	50	59.5	

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation	<input type="text" value="280"/> m
Minimum Catchment Elevation	<input type="text" value="266"/> m
Catchment length	<input type="text" value="700"/> m
Catchment Slope	<input type="text" value="2%"/>
Catchment Area	<input type="text" value="29.42"/> ha

Time of Concentration (Minutes)	<input type="text" value="24.77"/>
Time of Concentration (Hours)	<input type="text" value="0.41"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.28"/>

Time to Peak	<input type="text" value="0.74"/> hrs
--------------	---------------------------------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation	<input type="text" value="280"/> m
Minimum Catchment Elevation	<input type="text" value="266"/> m
Catchment length	<input type="text" value="700"/> m
Catchment Slope	<input type="text" value="2%"/>
Catchment Area	<input type="text" value="29.42"/> ha

Time of Concentration (Minutes)	<input type="text" value="66.15"/>
Time of Concentration (Hours)	<input type="text" value="1.10"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.74"/>

Initial Abstraction	<input type="text" value="5.5"/> mm
---------------------	-------------------------------------

Wetlands	<input type="text" value="12"/>
Woods	<input type="text" value="10"/>
Meadows	<input type="text" value="8"/>
Gravel	<input type="text" value="3"/>
Lawns	<input type="text" value="5"/>
Impervious	<input type="text" value="2"/>

Runoff Coefficient	<input type="text" value="0.14"/>
--------------------	-----------------------------------

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.136	#N/A	#N/A	#N/A	#N/A



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Collingwood Bracebridge Orillia Barrie

Project:	Buris Creek Event Grounds
File No.:	115032
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Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

Buris Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel		Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type	
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent		CN
gus	GUERIN	AB	Sand Loam	1	42.47	1	33.55	0.79	46	8.494	0.2	59	0	0	51	0	0	89	0.425	0.01	100	0	0	50	49.14
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
ans	ALLUSTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0
Totals					42.47	1	33.5513	0.79	46	8.494	0.2	59	0	0	51	0	0	89	0.4247	0.01	100	0	0	50	49.1

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction mm

Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.093	#N/A	#N/A	#N/A	#N/A



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Checked By:	ALK
Subject:	CN Calculator

Burls Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																												
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland				Pasture/Lawns				Meadows				Gravel		Impervious				Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN				
gus	GUERIN	AB	Sand Loam	1	38.86	1	7.772	0.2	46	29.15	0.75	59	0	0	51	1.943	0.05	89	0	0	100	0	0	50	57.9			
stsl	SARGENT	AB	Sand Loam	1	0		0		46	0		59	0		51	0		89	0		100	0		50	0			
vsl	VASEY	AB	Sand Loam	1	0		0		46	0		59	0		51	0		89	0		100	0		50	0			
ans	ALLISTON	AB	Sand Loam	1	0		0		46	0		59	0		51	0		89	0		100	0		50	0			
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0		#N/A	0			
Totals					38.86	1	7.772	0.2	46	29.15	0.75	59	0	0	51	1.943	0.05	89	0	0	100	0	0	50	57.9			

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction mm

Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.121	#N/A	#N/A	#N/A	#N/A



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Buris Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
gus	GUERIN	AB	Sand Loam	1	17.49	1	15.74	0.9	46	1.399	0.08	59	0	51	0.175	0.01	89	0.175	0.01	100	0	50	46.01		
stsl	SARGENT	AB	Sand Loam	1	0	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	0			
vasl	VASEY	AB	Sand Loam	1	0	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	0			
ans	ALLISTON	AB	Sand Loam	1	0	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	0			
	#N/A	#N/A	#N/A	#N/A	0	0	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0		
Totals					17.49	1	15.741	0.9	46	1.3992	0.08	59	0	51	0.1749	0.01	89	0.1749	0.01	100	0	50	46.0		

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation	<input type="text" value="272"/> m
Minimum Catchment Elevation	<input type="text" value="258"/> m
Catchment length	<input type="text" value="1500"/> m
Catchment Slope	<input type="text" value="1%"/>
Catchment Area	<input type="text" value="17.49"/> ha

Time of Concentration (Minutes)	<input type="text" value="65.11"/>
Time of Concentration (Hours)	<input type="text" value="1.09"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.72"/>

Time to Peak	<input type="text" value="1.44"/> hrs
--------------	---------------------------------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation	<input type="text" value="272"/> m
Minimum Catchment Elevation	<input type="text" value="258"/> m
Catchment length	<input type="text" value="1500"/> m
Catchment Slope	<input type="text" value="1%"/>
Catchment Area	<input type="text" value="17.49"/> ha

Time of Concentration (Minutes)	<input type="text" value="129.75"/>
Time of Concentration (Hours)	<input type="text" value="2.16"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="1.44"/>

Initial Abstraction	<input type="text" value="9.45"/> mm
---------------------	--------------------------------------

Wetlands	<input type="text" value="12"/>
Woods	<input type="text" value="10"/>
Meadows	<input type="text" value="8"/>
Gravel	<input type="text" value="3"/>
Lawns	<input type="text" value="5"/>
Impervious	<input type="text" value="2"/>

Runoff Coefficient	<input type="text" value="0.10"/>
--------------------	-----------------------------------

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.096	#N/A	#N/A	#N/A	#N/A



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Burls Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows		Gravel			Impervious			Wetland/Lakes/SWMP			Average CN for Soil Type	
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent		CN
gus	GUERIN	AB	Sand Loam	1	20.82	1	4.164	0.2	46	11.45	0.55	59	0	0	51	4.997	0.24	89	0.208	0.01	100	0	0	50	64.01
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0
Totals					20.82	1	4.164	0.2	46	11.451	0.55	59	0	0	51	4.9968	0.24	89	0.2062	0.01	100	0	0	50	64.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak	0.79 hrs
--------------	----------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction	5.48 mm
Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient	0.22
--------------------	------

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMP	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.225	#N/A	#N/A	#N/A	#N/A

```

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U A A A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

OOO TTTTT TTTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
OOO T T H H Y M M OOO

```

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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files\Visual OTTHYMO 2.2.4\voin.dat
 Output filename: I:\2015PR~1\115032~1\Design\SWM\OTTHYM~1\Existing CHI.out
 Summary filename: I:\2015PR~1\115032~1\Design\SWM\OTTHYM~1\Existing CHI.sum

DATE: 6/4/2015 TIME: 9:12:55 AM

USER:

Existing Condition Chicago Design Storm

COMMENTS:

 ** SIMULATION NUMBER: 1 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
	START @ .00 hrs								

	READ STORM		10.0						
	[Ptot= 33.84 mm]								
	fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 2-yr Orillia.stm								
	remark: 2-Year Orillia 4-hour Chicago Storm								
*									
**	CALIB NASHYD	0302	1 5.0	115.98	.41	3.17	4.17	.12	.000
	[CN=64.3]								
	[N = 3.0:Tp 1.32]								
*									
**	CALIB NASHYD	0301	1 5.0	212.69	.38	4.67	3.37	.10	.000
	[CN=57.8]								
	[N = 3.0:Tp 2.55]								
*									
**	CALIB NASHYD	0101	1 5.0	79.63	.40	2.67	4.87	.14	.000
	[CN=67.7]								
	[N = 3.0:Tp .98]								
*									
**	CALIB NASHYD	0104	1 5.0	38.86	.16	2.50	3.67	.11	.000
	[CN=57.9]								
	[N = 3.0:Tp .88]								
*									
**	CALIB NASHYD	0305	1 5.0	18.93	.03	4.67	3.37	.10	.000
	[CN=57.8]								
	[N = 3.0:Tp 2.55]								
*									
**	CALIB NASHYD	0303	1 5.0	162.73	.38	3.50	3.12	.09	.000
	[CN=56.8]								
	[N = 3.0:Tp 1.56]								
*									
*	CALIB STANDHYD	0304	1 5.0	46.90	1.63	1.42	13.59	.40	.000
	[I%=20.0:S%= 2.00]								
*									
*	CALIB NASHYD	0306	1 5.0	127.89	.44	4.58	6.39	.19	.000
	[CN=75.7]								
	[N = 3.0:Tp 2.51]								
*									
*	CALIB NASHYD	0307	1 5.0	191.06	.66	4.58	6.39	.19	.000
	[CN=75.7]								
	[N = 3.0:Tp 2.51]								
*									
*	CALIB NASHYD	0105	1 5.0	17.49	.03	3.42	1.99	.06	.000
	[CN=48.0]								
	[N = 3.0:Tp 1.44]								
*									
*	CALIB NASHYD	0103	1 5.0	42.47	.08	3.08	2.15	.06	.000

	[CN=49.1									
	[N = 3.0:Tp	1.19]								
*										
*	CALIB NASHYD	0102	1	5.0	29.42	.15	2.33	3.99	.12	.000
	[CN=59.5									
	[N = 3.0:Tp	.74]								
*										
*	CALIB NASHYD	0106	1	5.0	20.82	.12	2.42	4.69	.14	.000
	[CN=64.0									
	[N = 3.0:Tp	.79]								
*										
*	CALIB NASHYD	0308	1	5.0	187.19	.65	4.58	6.39	.19	.000
	[CN=75.7									
	[N = 3.0:Tp	2.51]								
*										
*	ADD [0301 + 0101]	3081	3	5.0	292.32	.64	3.33	3.78	n/a	.000
*										
*	ADD [3081 + 0104]	3051	3	5.0	331.18	.77	3.00	3.77	n/a	.000
*										
*	ADD [3051 + 0305]	3052	3	5.0	350.11	.80	3.08	3.74	n/a	.000
*										
*	ADD [0306 + 0307]	3082	3	5.0	318.95	1.10	4.58	6.39	n/a	.000
*										
*	ADD [0102 + 0106]	0310	3	5.0	50.24	.27	2.33	4.28	n/a	.000
*										
*	ADD [0302 + 3052]	0311	3	5.0	466.09	1.21	3.08	3.85	n/a	.000
*										
*	ADD [0103 + 0310]	3071	3	5.0	92.71	.34	2.42	3.31	n/a	.000
*										
*	ADD [0311 + 0303]	0313	3	5.0	628.82	1.58	3.25	3.66	n/a	.000
*										
*	ADD [0105 + 3071]	3061	3	5.0	110.20	.36	2.50	3.10	n/a	.000
*										
*	ADD [0313 + 0304]	0314	3	5.0	675.72	1.85	2.92	4.35	n/a	.000
*										
*	ADD [3082 + 3061]	3083	3	5.0	429.15	1.27	4.25	5.54	n/a	.000
*										
*	ADD [3083 + 0308]	3084	3	5.0	616.34	1.91	4.33	5.80	n/a	.000

 ** SIMULATION NUMBER: 2 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
-----	---------	--------	--------	---------	-----------	-----------	---------	------	-----------

START @ .00 hrs

READ STORM 10.0
 [Ptot= 44.10 mm]
 fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 5-yr Orillia.stm
 remark: 5-Year Orillia 4-hour Chicago Storm

**	CALIB NASHYD	0302	1	5.0	115.98	.77	3.08	7.58	.17	.000
	[CN=64.3									
	[N = 3.0:Tp	1.32]								
*										
**	CALIB NASHYD	0301	1	5.0	212.69	.70	4.58	6.15	.14	.000
	[CN=57.8									
	[N = 3.0:Tp	2.55]								
*										
**	CALIB NASHYD	0101	1	5.0	79.63	.75	2.58	8.69	.20	.000
	[CN=67.7									
	[N = 3.0:Tp	.98]								
*										
**	CALIB NASHYD	0104	1	5.0	38.86	.30	2.50	6.54	.15	.000
	[CN=57.9									
	[N = 3.0:Tp	.88]								
*										
**	CALIB NASHYD	0305	1	5.0	18.93	.06	4.58	6.15	.14	.000
	[CN=57.8									
	[N = 3.0:Tp	2.55]								
*										
**	CALIB NASHYD	0303	1	5.0	162.73	.72	3.42	5.77	.13	.000
	[CN=56.8									
	[N = 3.0:Tp	1.56]								
*										
*	CALIB STANDHYD	0304	1	5.0	46.90	2.53	1.33	20.30	.46	.000
	[I%=20.0:S%=	2.00]								
*										
*	CALIB NASHYD	0306	1	5.0	127.89	.79	4.50	11.28	.26	.000
	[CN=75.7									
	[N = 3.0:Tp	2.51]								
*										
*	CALIB NASHYD	0307	1	5.0	191.06	1.17	4.50	11.28	.26	.000
	[CN=75.7									
	[N = 3.0:Tp	2.51]								
*										
*	CALIB NASHYD	0105	1	5.0	17.49	.05	3.33	3.87	.09	.000

ID	TYPE	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
[CN=48.0 [N = 3.0:Tp 1.44]								
* CALIB NASHYD 0103	1	5.0	42.47	.16	2.92	4.15	.09	.000
[CN=49.1 [N = 3.0:Tp 1.19]								
* CALIB NASHYD 0102	1	5.0	29.42	.27	2.25	7.04	.16	.000
[CN=59.5 [N = 3.0:Tp .74]								
* CALIB NASHYD 0106	1	5.0	20.82	.22	2.33	8.21	.19	.000
[CN=64.0 [N = 3.0:Tp .79]								
* CALIB NASHYD 0308	1	5.0	187.19	1.15	4.50	11.28	.26	.000
[CN=75.7 [N = 3.0:Tp 2.51]								
ADD [0301 + 0101]	3081	3	5.0	292.32	1.18	3.17	6.84	n/a .000
ADD [3081 + 0104]	3051	3	5.0	331.18	1.43	2.92	6.81	n/a .000
ADD [3051 + 0305]	3052	3	5.0	350.11	1.47	3.00	6.77	n/a .000
ADD [0306 + 0307]	3082	3	5.0	318.95	1.96	4.50	11.28	n/a .000
ADD [0102 + 0106]	0310	3	5.0	50.24	.49	2.33	7.52	n/a .000
ADD [0302 + 3052]	0311	3	5.0	466.09	2.23	3.00	6.97	n/a .000
ADD [0103 + 0310]	3071	3	5.0	92.71	.63	2.42	5.98	n/a .000
ADD [0311 + 0303]	0313	3	5.0	628.82	2.93	3.17	6.66	n/a .000
ADD [0105 + 3071]	3061	3	5.0	110.20	.67	2.42	5.64	n/a .000
ADD [0313 + 0304]	0314	3	5.0	675.72	3.29	2.92	7.61	n/a .000
ADD [3082 + 3061]	3083	3	5.0	429.15	2.27	4.17	9.84	n/a .000
ADD [3083 + 0308]	3084	3	5.0	616.34	3.41	4.25	10.28	n/a .000

 ** SIMULATION NUMBER: 3 **

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ .00 hrs								

READ STORM		10.0						
[Ptot= 50.61 mm]								
fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 10-yr Orillia.stm								
remark: 10-Year Orillia 4-hour Chicago Storm								
** CALIB NASHYD 0302	1	5.0	115.98	1.03	3.00	10.13	.20	.000
[CN=64.3 [N = 3.0:Tp 1.32]								
** CALIB NASHYD 0301	1	5.0	212.69	.94	4.50	8.27	.16	.000
[CN=57.8 [N = 3.0:Tp 2.55]								
** CALIB NASHYD 0101	1	5.0	79.63	1.01	2.58	11.54	.23	.000
[CN=67.7 [N = 3.0:Tp .98]								
** CALIB NASHYD 0104	1	5.0	38.86	.40	2.42	8.71	.17	.000
[CN=57.9 [N = 3.0:Tp .88]								
** CALIB NASHYD 0305	1	5.0	18.93	.08	4.50	8.27	.16	.000
[CN=57.8 [N = 3.0:Tp 2.55]								
** CALIB NASHYD 0303	1	5.0	162.73	.98	3.42	7.80	.15	.000
[CN=56.8 [N = 3.0:Tp 1.56]								
* CALIB STANDHYD 0304	1	5.0	46.90	3.10	1.33	24.92	.49	.000
[I%=20.0:S%= 2.00]								
* CALIB NASHYD 0306	1	5.0	127.89	1.04	4.42	14.85	.29	.000
[CN=75.7 [N = 3.0:Tp 2.51]								
* CALIB NASHYD 0307	1	5.0	191.06	1.55	4.42	14.85	.29	.000

	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0105	1	5.0	17.49	.08	3.25	5.36	.11	.000
	[CN=48.0]									
	[N = 3.0:Tp 1.44]									
*										
*	CALIB NASHYD	0103	1	5.0	42.47	.23	2.92	5.70	.11	.000
	[CN=49.1]									
	[N = 3.0:Tp 1.19]									
*										
*	CALIB NASHYD	0102	1	5.0	29.42	.37	2.25	9.33	.18	.000
	[CN=59.5]									
	[N = 3.0:Tp .74]									
*										
*	CALIB NASHYD	0106	1	5.0	20.82	.29	2.33	10.83	.21	.000
	[CN=64.0]									
	[N = 3.0:Tp .79]									
*										
*	CALIB NASHYD	0308	1	5.0	187.19	1.52	4.42	14.85	.29	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*										
*	ADD [0301 + 0101]	3081	3	5.0	292.32	1.58	3.08	9.16	n/a	.000
*										
*	ADD [3081 + 0104]	3051	3	5.0	331.18	1.93	2.92	9.11	n/a	.000
*										
*	ADD [3051 + 0305]	3052	3	5.0	350.11	1.98	2.92	9.06	n/a	.000
*										
*	ADD [0306 + 0307]	3082	3	5.0	318.95	2.59	4.42	14.85	n/a	.000
*										
*	ADD [0102 + 0106]	0310	3	5.0	50.24	.66	2.25	9.95	n/a	.000
*										
*	ADD [0302 + 3052]	0311	3	5.0	466.09	3.01	3.00	9.33	n/a	.000
*										
*	ADD [0103 + 0310]	3071	3	5.0	92.71	.85	2.42	8.00	n/a	.000
*										
*	ADD [0311 + 0303]	0313	3	5.0	628.82	3.97	3.08	8.93	n/a	.000
*										
*	ADD [0105 + 3071]	3061	3	5.0	110.20	.91	2.42	7.58	n/a	.000
*										
*	ADD [0313 + 0304]	0314	3	5.0	675.72	4.39	2.92	10.04	n/a	.000
*										
*	ADD [3082 + 3061]	3083	3	5.0	429.15	3.00	4.08	12.99	n/a	.000
*										
*	ADD [3083 + 0308]	3084	3	5.0	616.34	4.50	4.17	13.55	n/a	.000

 ** SIMULATION NUMBER: 4 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms	
	START @ .00 hrs									

	READ STORM		10.0							
	[Ptot= 58.97 mm]									
	fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 25-yr Orillia.stm									
	remark: 25-Year Orillia 4-hour Chicago Storm									
*										
**	CALIB NASHYD	0302	1	5.0	115.98	1.43	3.00	13.81	.23	.000
	[CN=64.3]									
	[N = 3.0:Tp 1.32]									
*										
**	CALIB NASHYD	0301	1	5.0	212.69	1.30	4.50	11.34	.19	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*										
**	CALIB NASHYD	0101	1	5.0	79.63	1.39	2.58	15.60	.26	.000
	[CN=67.7]									
	[N = 3.0:Tp .98]									
*										
**	CALIB NASHYD	0104	1	5.0	38.86	.55	2.42	11.84	.20	.000
	[CN=57.9]									
	[N = 3.0:Tp .88]									
*										
**	CALIB NASHYD	0305	1	5.0	18.93	.12	4.50	11.34	.19	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*										
**	CALIB NASHYD	0303	1	5.0	162.73	1.37	3.33	10.75	.18	.000
	[CN=56.8]									
	[N = 3.0:Tp 1.56]									
*										
*	CALIB STANDHYD	0304	1	5.0	46.90	3.88	1.33	31.14	.53	.000
	[I%=20.0:S%= 2.00]									
*										
*	CALIB NASHYD	0306	1	5.0	127.89	1.39	4.42	19.86	.34	.000

CALIB STANDHYD	0304	1	5.0	46.90	5.22	1.50	36.22	.55	.000	
[I%=20.0:S%= 2.00]										
CALIB NASHYD	0306	1	5.0	127.89	1.69	4.33	24.05	.37	.000	
[CN=75.7 [N = 3.0:Tp 2.51]										
CALIB NASHYD	0307	1	5.0	191.06	2.53	4.33	24.05	.37	.000	
[CN=75.7 [N = 3.0:Tp 2.51]										
CALIB NASHYD	0105	1	5.0	17.49	.14	3.17	9.49	.14	.000	
[CN=48.0 [N = 3.0:Tp 1.44]										
CALIB NASHYD	0103	1	5.0	42.47	.41	2.83	10.01	.15	.000	
[CN=49.1 [N = 3.0:Tp 1.19]										
CALIB NASHYD	0102	1	5.0	29.42	.63	2.25	15.46	.24	.000	
[CN=59.5 [N = 3.0:Tp .74]										
CALIB NASHYD	0106	1	5.0	20.82	.49	2.33	17.76	.27	.000	
[CN=64.0 [N = 3.0:Tp .79]										
CALIB NASHYD	0308	1	5.0	187.19	2.48	4.33	24.05	.37	.000	
[CN=75.7 [N = 3.0:Tp 2.51]										
ADD [0301 + 0101]	3081	3	5.0	292.32	2.69	3.08	15.37	n/a	.000	
ADD [3081 + 0104]	3051	3	5.0	331.18	3.28	2.83	15.28	n/a	.000	
ADD [3051 + 0305]	3052	3	5.0	350.11	3.37	2.83	15.21	n/a	.000	
ADD [0306 + 0307]	3082	3	5.0	318.95	4.22	4.33	24.05	n/a	.000	
ADD [0102 + 0106]	0310	3	5.0	50.24	1.12	2.25	16.41	n/a	.000	
ADD [0302 + 3052]	0311	3	5.0	466.09	5.14	2.92	15.64	n/a	.000	
ADD [0103 + 0310]	3071	3	5.0	92.71	1.47	2.33	13.48	n/a	.000	
ADD [0311 + 0303]	0313	3	5.0	628.82	6.80	3.00	15.04	n/a	.000	
ADD [0105 + 3071]	3061	3	5.0	110.20	1.57	2.42	12.85	n/a	.000	
ADD [0313 + 0304]	0314	3	5.0	675.72	7.34	2.92	16.51	n/a	.000	
ADD [3082 + 3061]	3083	3	5.0	429.15	4.93	4.00	21.18	n/a	.000	
ADD [3083 + 0308]	3084	3	5.0	616.34	7.37	4.08	22.05	n/a	.000	

 ** SIMULATION NUMBER: 6 **

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms		
START @ .00 hrs										

READ STORM		10.0								
[Ptot= 71.71 mm]										
fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 100-yr Orillia.stm										
remark: 100-Year Orillia 4-hour Chicago Storm										
CALIB NASHYD	0302	1	5.0	115.98	2.11	3.00	20.14	.28		
[CN=64.3 [N = 3.0:Tp 1.32]										
CALIB NASHYD	0301	1	5.0	212.69	1.92	4.42	16.69	.23		
[CN=57.8 [N = 3.0:Tp 2.55]										
CALIB NASHYD	0101	1	5.0	79.63	2.04	2.50	22.52	.31		
[CN=67.7 [N = 3.0:Tp .98]										
CALIB NASHYD	0104	1	5.0	38.86	.82	2.42	17.28	.24		
[CN=57.9 [N = 3.0:Tp .88]										
CALIB NASHYD	0305	1	5.0	18.93	.17	4.42	16.69	.23		
[CN=57.8 [N = 3.0:Tp 2.55]										

**	CALIB NASHYD	0305	1	5.0	18.93	.63	10.83	93.06	.48	.000
	[CN=57.8									
	[N = 3.0:Tp 2.55]									
*										
**	CALIB NASHYD	0303	1	5.0	162.73	6.29	9.50	90.72	.47	.000
	[CN=56.8									
	[N = 3.0:Tp 1.56]									
*										
*	CALIB STANDHYD	0304	1	5.0	46.90	4.61	7.00	150.32	.78	.000
	[I%=20.0:S%= 2.00]									
*										
*	CALIB NASHYD	0306	1	5.0	127.89	5.83	10.42	128.77	.67	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0307	1	5.0	191.06	8.70	10.42	128.77	.67	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0105	1	5.0	17.49	.56	9.42	73.45	.38	.000
	[CN=48.0									
	[N = 3.0:Tp 1.44]									
*										
*	CALIB NASHYD	0103	1	5.0	42.47	1.45	9.25	75.74	.39	.000
	[CN=49.1									
	[N = 3.0:Tp 1.19]									
*										
*	CALIB NASHYD	0102	1	5.0	29.42	1.54	7.42	97.53	.51	.000
	[CN=59.5									
	[N = 3.0:Tp .74]									
*										
*	CALIB NASHYD	0106	1	5.0	20.82	1.16	7.50	106.42	.55	.000
	[CN=64.0									
	[N = 3.0:Tp .79]									
*										
*	CALIB NASHYD	0308	1	5.0	187.19	8.53	10.42	128.77	.67	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
*	ADD [0301 + 0101]	3081	3	5.0	292.32	10.26	9.67	98.39	n/a	.000
*										
*	ADD [3081 + 0104]	3051	3	5.0	331.18	11.80	9.50	97.89	n/a	.000
*										
*	ADD [3051 + 0305]	3052	3	5.0	350.11	12.37	9.58	97.63	n/a	.000
*										
*	ADD [0306 + 0307]	3082	3	5.0	318.95	14.53	10.42	128.77	n/a	.000
*										
*	ADD [0102 + 0106]	0310	3	5.0	50.24	2.70	7.50	101.22	n/a	.000
*										
*	ADD [0302 + 3052]	0311	3	5.0	466.09	17.67	9.42	99.58	n/a	.000
*										
*	ADD [0103 + 0310]	3071	3	5.0	92.71	3.96	7.67	89.55	n/a	.000
*										
*	ADD [0311 + 0303]	0313	3	5.0	628.82	23.96	9.42	97.29	n/a	.000
*										
*	ADD [0105 + 3071]	3061	3	5.0	110.20	4.40	7.75	86.99	n/a	.000
*										
*	ADD [0313 + 0304]	0314	3	5.0	675.72	26.31	9.17	100.97	n/a	.000
*										
*	ADD [3082 + 3061]	3083	3	5.0	429.15	18.09	9.92	118.04	n/a	.000
*										
*	ADD [3083 + 0308]	3084	3	5.0	616.34	26.53	10.08	121.30	n/a	.000
*										

FINISH
 =====

*	CALIB NASHYD	0105	1	5.0	17.49	.04	13.75	4.60	.10	.000
	[CN=48.0]									
	[N = 3.0:Tp 1.44]									
*	CALIB NASHYD	0307	1	5.0	191.06	.91	15.17	13.06	.28	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*	CALIB NASHYD	0306	1	5.0	127.89	.61	15.17	13.06	.28	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*	ADD [0101 + 0301]	3081	3	5.0	292.32	.86	13.58	7.99	n/a	.000
*	ADD [0106 + 0102]	0310	3	5.0	50.24	.34	12.83	8.72	n/a	.000
*	ADD [0310 + 0103]	3071	3	5.0	92.71	.44	13.00	6.97	n/a	.000
*	ADD [3071 + 0105]	3061	3	5.0	110.20	.47	13.00	6.60	n/a	.000
*	ADD [0307 + 0306]	3082	3	5.0	318.95	1.52	15.17	13.06	n/a	.000
*	ADD [0104 + 3081]	3051	3	5.0	331.18	1.05	13.33	7.94	n/a	.000
*	ADD [3061 + 3082]	3083	3	5.0	429.15	1.75	14.83	11.40	n/a	.000
*	ADD [0305 + 3051]	3052	3	5.0	350.11	1.08	13.42	7.90	n/a	.000
*	ADD [0308 + 3083]	3084	3	5.0	616.34	2.63	15.00	11.90	n/a	.000
*	ADD [3052 + 0302]	0311	3	5.0	466.09	1.63	13.42	8.13	n/a	.000
*	ADD [0303 + 0311]	0313	3	5.0	628.82	2.14	13.58	7.78	n/a	.000
*	ADD [0304 + 0313]	0314	3	5.0	675.72	2.53	13.08	8.81	n/a	.000

 ** SIMULATION NUMBER: 2 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms	
	START @ .00 hrs									

	MASS STORM		20.0							
	[Ptot= 61.80 mm]									
*	CALIB STANDHYD	0304	1	5.0	46.90	1.84	12.08	33.32	.54	.000
	[I%=20.0:S%= 2.00]									
*	CALIB NASHYD	0303	1	5.0	162.73	.94	13.83	11.84	.19	.000
	[CN=56.8]									
	[N = 3.0:Tp 1.56]									
*	CALIB NASHYD	0305	1	5.0	18.93	.08	15.25	12.46	.20	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*	CALIB NASHYD	0104	1	5.0	38.86	.36	13.00	12.98	.21	.000
	[CN=57.9]									
	[N = 3.0:Tp .88]									
*	CALIB NASHYD	0101	1	5.0	79.63	.94	13.08	17.06	.28	.000
	[CN=67.7]									
	[N = 3.0:Tp .98]									
*	CALIB NASHYD	0301	1	5.0	212.69	.94	15.25	12.46	.20	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*	CALIB NASHYD	0302	1	5.0	115.98	.98	13.50	15.14	.25	.000
	[CN=64.3]									
	[N = 3.0:Tp 1.32]									
*	CALIB NASHYD	0308	1	5.0	187.19	1.51	15.08	21.64	.35	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*	CALIB NASHYD	0106	1	5.0	20.82	.26	12.83	15.92	.26	.000
	[CN=64.0]									
	[N = 3.0:Tp .79]									
*	CALIB NASHYD	0102	1	5.0	29.42	.32	12.75	13.82	.22	.000
	[CN=59.5]									
	[N = 3.0:Tp .74]									
*	CALIB NASHYD	0103	1	5.0	42.47	.22	13.33	8.84	.14	.000

*	CALIB NASHYD	0103	1	5.0	42.47	.30	13.33	11.95	.17	.000
	[CN=49.1]								
	[N = 3.0:Tp	1.19]								
*	CALIB NASHYD	0105	1	5.0	17.49	.10	13.67	11.35	.16	.000
	[CN=48.0]								
	[N = 3.0:Tp	1.44]								
*	CALIB NASHYD	0307	1	5.0	191.06	2.01	15.00	27.94	.39	.000
	[CN=75.7]								
	[N = 3.0:Tp	2.51]								
*	CALIB NASHYD	0306	1	5.0	127.89	1.34	15.00	27.94	.39	.000
	[CN=75.7]								
	[N = 3.0:Tp	2.51]								
*	ADD [0101 + 0301]	3081	3	5.0	292.32	2.02	13.50	18.08	n/a	.000
*	ADD [0106 + 0102]	0310	3	5.0	50.24	.77	12.83	19.22	n/a	.000
*	ADD [0310 + 0103]	3071	3	5.0	92.71	1.03	12.92	15.89	n/a	.000
*	ADD [3071 + 0105]	3061	3	5.0	110.20	1.12	13.00	15.17	n/a	.000
*	ADD [0307 + 0306]	3082	3	5.0	318.95	3.35	15.00	27.94	n/a	.000
*	ADD [0104 + 3081]	3051	3	5.0	331.18	2.46	13.33	17.97	n/a	.000
*	ADD [3061 + 3082]	3083	3	5.0	429.15	3.92	14.67	24.66	n/a	.000
*	ADD [0305 + 3051]	3052	3	5.0	350.11	2.53	13.33	17.89	n/a	.000
*	ADD [0308 + 3083]	3084	3	5.0	616.34	5.87	14.75	25.66	n/a	.000
*	ADD [3052 + 0302]	0311	3	5.0	466.09	3.83	13.42	18.40	n/a	.000
*	ADD [0303 + 0311]	0313	3	5.0	628.82	5.06	13.50	17.71	n/a	.000
*	ADD [0304 + 0313]	0314	3	5.0	675.72	5.70	13.08	19.32	n/a	.000

** SIMULATION NUMBER: 4 **

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms
	START @									
	.00 hrs									

	MASS STORM			20.0						
	[Ptot= 83.30 mm]									
*	CALIB STANDHYD	0304	1	5.0	46.90	2.95	12.08	50.69	.61	.000
	[I%=20.0:S%= 2.00]									
*	CALIB NASHYD	0303	1	5.0	162.73	1.73	13.75	21.26	.26	.000
	[CN=56.8]								
	[N = 3.0:Tp	1.56]								
*	CALIB NASHYD	0305	1	5.0	18.93	.15	15.17	22.19	.27	.000
	[CN=57.8]								
	[N = 3.0:Tp	2.55]								
*	CALIB NASHYD	0104	1	5.0	38.86	.65	12.92	22.85	.27	.000
	[CN=57.9]								
	[N = 3.0:Tp	.88]								
*	CALIB NASHYD	0101	1	5.0	79.63	1.65	13.08	29.48	.35	.000
	[CN=67.7]								
	[N = 3.0:Tp	.98]								
*	CALIB NASHYD	0301	1	5.0	212.69	1.71	15.17	22.19	.27	.000
	[CN=57.8]								
	[N = 3.0:Tp	2.55]								
*	CALIB NASHYD	0302	1	5.0	115.98	1.76	13.42	26.56	.32	.000
	[CN=64.3]								
	[N = 3.0:Tp	1.32]								
*	CALIB NASHYD	0308	1	5.0	187.19	2.59	15.00	36.45	.44	.000
	[CN=75.7]								
	[N = 3.0:Tp	2.51]								
*	CALIB NASHYD	0106	1	5.0	20.82	.45	12.83	27.43	.33	.000
	[CN=64.0]								
	[N = 3.0:Tp	.79]								
*	CALIB NASHYD	0102	1	5.0	29.42	.58	12.75	24.13	.29	.000

*	CALIB NASHYD [CN=59.5 [N = 3.0:Tp .74]	0102	1	5.0	29.42	.70	12.75	28.95	.31	.000
*	CALIB NASHYD [CN=49.1 [N = 3.0:Tp 1.19]	0103	1	5.0	42.47	.51	13.33	20.01	.22	.000
*	CALIB NASHYD [CN=48.0 [N = 3.0:Tp 1.44]	0105	1	5.0	17.49	.17	13.58	19.13	.21	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0307	1	5.0	191.06	3.14	14.92	43.08	.47	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0306	1	5.0	127.89	2.10	14.92	43.08	.47	.000
*	ADD [0101 + 0301]	3081	3	5.0	292.32	3.30	13.50	29.06	n/a	.000
*	ADD [0106 + 0102]	0310	3	5.0	50.24	1.24	12.75	30.52	n/a	.000
*	ADD [0310 + 0103]	3071	3	5.0	92.71	1.69	12.92	25.71	n/a	.000
*	ADD [3071 + 0105]	3061	3	5.0	110.20	1.83	12.92	24.66	n/a	.000
*	ADD [0307 + 0306]	3082	3	5.0	318.95	5.24	14.92	43.08	n/a	.000
*	ADD [0104 + 3081]	3051	3	5.0	331.18	4.01	13.33	28.87	n/a	.000
*	ADD [3061 + 3082]	3083	3	5.0	429.15	6.19	14.58	38.35	n/a	.000
*	ADD [0305 + 3051]	3052	3	5.0	350.11	4.13	13.33	28.76	n/a	.000
*	ADD [0308 + 3083]	3084	3	5.0	616.34	9.23	14.67	39.79	n/a	.000
*	ADD [3052 + 0302]	0311	3	5.0	466.09	6.25	13.33	29.53	n/a	.000
*	ADD [0303 + 0311]	0313	3	5.0	628.82	8.30	13.42	28.54	n/a	.000
*	ADD [0304 + 0313]	0314	3	5.0	675.72	9.10	13.08	30.60	n/a	.000

** SIMULATION NUMBER: 6 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms	
	START @ .00 hrs									

	MASS STORM		20.0							
	[Ptot=101.10 mm]									
*	CALIB STANDHYD [I%=20.0:S%= 2.00]	0304	1	5.0	46.90	4.19	12.08	65.92	.65	.000
*	CALIB NASHYD [CN=56.8 [N = 3.0:Tp 1.56]	0303	1	5.0	162.73	2.50	13.75	30.44	.30	.000
*	CALIB NASHYD [CN=57.8 [N = 3.0:Tp 2.55]	0305	1	5.0	18.93	.22	15.08	31.62	.31	.000
*	CALIB NASHYD [CN=57.9 [N = 3.0:Tp .88]	0104	1	5.0	38.86	.93	12.92	32.38	.32	.000
*	CALIB NASHYD [CN=67.7 [N = 3.0:Tp .98]	0101	1	5.0	79.63	2.33	13.00	41.13	.41	.000
*	CALIB NASHYD [CN=57.8 [N = 3.0:Tp 2.55]	0301	1	5.0	212.69	2.46	15.08	31.62	.31	.000
*	CALIB NASHYD [CN=64.3 [N = 3.0:Tp 1.32]	0302	1	5.0	115.98	2.51	13.42	37.40	.37	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0308	1	5.0	187.19	3.58	14.92	49.95	.49	.000
*	CALIB NASHYD	0106	1	5.0	20.82	.64	12.83	38.33	.38	.000

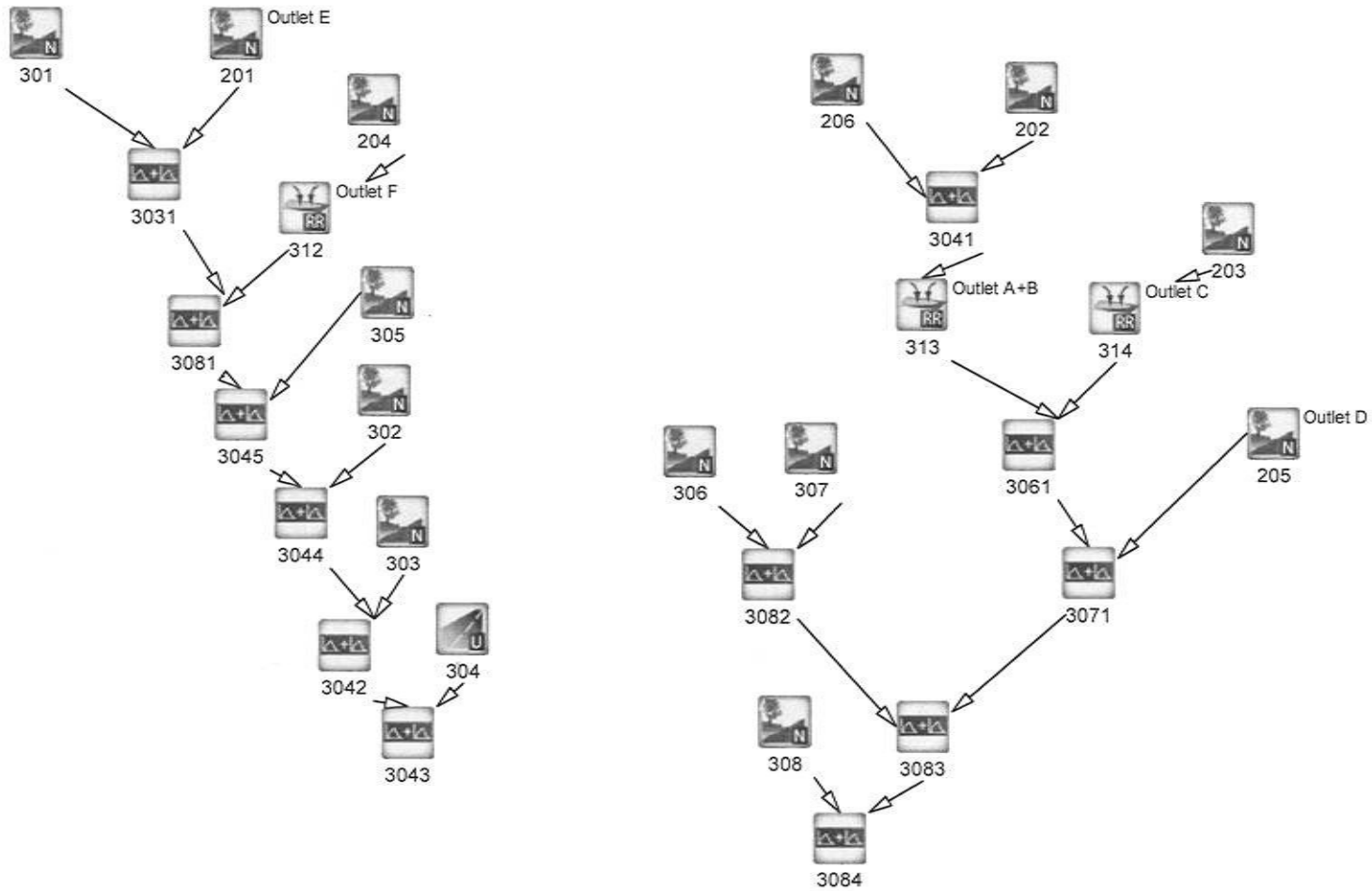
	[CN=64.0 [N = 3.0:Tp .79]									
*	CALIB NASHYD	0102	1	5.0	29.42	.82	12.75	34.03	.34	.000
	[CN=59.5 [N = 3.0:Tp .74]									
*	CALIB NASHYD	0103	1	5.0	42.47	.61	13.33	23.90	.24	.000
	[CN=49.1 [N = 3.0:Tp 1.19]									
*	CALIB NASHYD	0105	1	5.0	17.49	.21	13.58	22.90	.23	.000
	[CN=48.0 [N = 3.0:Tp 1.44]									
*	CALIB NASHYD	0307	1	5.0	191.06	3.65	14.92	49.95	.49	.000
	[CN=75.7 [N = 3.0:Tp 2.51]									
*	CALIB NASHYD	0306	1	5.0	127.89	2.45	14.92	49.95	.49	.000
	[CN=75.7 [N = 3.0:Tp 2.51]									
*	ADD [0101 + 0301]	3081	3	5.0	292.32	3.90	13.50	34.21	n/a	.000
*	ADD [0106 + 0102]	0310	3	5.0	50.24	1.46	12.75	35.81	n/a	.000
*	ADD [0310 + 0103]	3071	3	5.0	92.71	2.00	12.92	30.36	n/a	.000
*	ADD [3071 + 0105]	3061	3	5.0	110.20	2.18	12.92	29.17	n/a	.000
*	ADD [0307 + 0306]	3082	3	5.0	318.95	6.10	14.92	49.95	n/a	.000
*	ADD [0104 + 3081]	3051	3	5.0	331.18	4.74	13.33	34.00	n/a	.000
*	ADD [3061 + 3082]	3083	3	5.0	429.15	7.23	14.50	44.61	n/a	.000
*	ADD [0305 + 3051]	3052	3	5.0	350.11	4.89	13.33	33.87	n/a	.000
*	ADD [0308 + 3083]	3084	3	5.0	616.34	10.77	14.67	46.23	n/a	.000
*	ADD [3052 + 0302]	0311	3	5.0	466.09	7.39	13.33	34.75	n/a	.000
*	ADD [0303 + 0311]	0313	3	5.0	628.82	9.83	13.42	33.63	n/a	.000
*	ADD [0304 + 0313]	0314	3	5.0	675.72	10.71	13.08	35.87	n/a	.000

FINISH

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**APPENDIX B:
POST-DEVELOPMENT HYDROLOGY CALCULATIONS**

Proposed Conditions OTTHYMO Model Schematic





Project:	Burls Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

Burls Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel			Impervious			Wetland/Lakes/SWMP			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
gus	GUERIN	AB	Sand Loam	1	71.81	1	4.309	0.06	46	60.32	0.84	59	0	0	51	5.027	0.07	89	2.154	0.03	100	0	0	50	61.55
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
vast	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	#N/A	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0
Totals					71.81	1	4.309	0.06	46	60.32	0.84	59	0	0	51	5.027	0.07	89	2.154	0.03	100	0	0	50	61.55

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak	<input type="text" value="1.07"/> hrs
--------------	---------------------------------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction	<input type="text" value="5.07"/> mm
---------------------	--------------------------------------

Wetlands	<input type="text" value="12"/>
Woods	<input type="text" value="10"/>
Meadows	<input type="text" value="8"/>
Gravel	<input type="text" value="3"/>
Lawns	<input type="text" value="5"/>
Impervious	<input type="text" value="2"/>

Runoff Coefficient	<input type="text" value="0.16"/>
--------------------	-----------------------------------

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMP	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.159	#N/A	#N/A	#N/A	#N/A



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie

Project:	Burls Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

Burls Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel		Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type	
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent		CN
gus	GUERIN	AB	Sand Loam	1	29.42	1	3.825	0.13	46	23.54	0.8	59	0	0	51	1.765	0.06	89	0.294	0.01	100	0	0	50	59.52
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0
Totals					29.42	1	3.8246	0.13	46	23.536	0.8	59	0	0	51	1.7652	0.06	89	0.2942	0.01	100	0	0	50	59.5

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction mm

Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.136	#N/A	#N/A	#N/A	#N/A



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie

Project:	BurIs Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

BurIs Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
gus	GUERIN	AB	Sand Loam	1	42.47	1	30.58	0.72	46	6.371	0.15	59	0	51	5.096	0.12	89	0.425	0.01	100	0	50	53.65		
stsl	SARGENT	AB	Sand Loam	1	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	50	0			
vasl	VASEY	AB	Sand Loam	1	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	50	0			
ans	ALLSTON	AB	Sand Loam	1	0	0	46	0	59	0	51	0	89	0	100	0	50	0	50	0	50	0			
	#N/A	#N/A	#N/A	#N/A	0	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0	#N/A	0			
Totals					42.47	1	30.5784	0.72	46	6.3705	0.15	59	0	51	5.0964	0.12	89	0.4247	0.01	100	0	50	53.7		

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation	<input type="text" value="280"/> m
Minimum Catchment Elevation	<input type="text" value="259"/> m
Catchment length	<input type="text" value="1400"/> m
Catchment Slope	<input type="text" value="2%"/>
Catchment Area	<input type="text" value="42.47"/> ha

Time of Concentration (Minutes)	<input type="text" value="50.58"/>
Time of Concentration (Hours)	<input type="text" value="0.84"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.56"/>

Time to Peak	<input type="text" value="1.12"/> hrs
--------------	---------------------------------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation	<input type="text" value="280"/> m
Minimum Catchment Elevation	<input type="text" value="259"/> m
Catchment length	<input type="text" value="1400"/> m
Catchment Slope	<input type="text" value="2%"/>
Catchment Area	<input type="text" value="42.47"/> ha

Time of Concentration (Minutes)	<input type="text" value="100.93"/>
Time of Concentration (Hours)	<input type="text" value="1.68"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="1.12"/>

Initial Abstraction	<input type="text" value="8.33"/> mm
---------------------	--------------------------------------

Wetlands	<input type="text" value="12"/>
Woods	<input type="text" value="10"/>
Meadows	<input type="text" value="8"/>
Gravel	<input type="text" value="3"/>
Lawns	<input type="text" value="5"/>
Impervious	<input type="text" value="2"/>

Runoff Coefficient	<input type="text" value="0.15"/>
--------------------	-----------------------------------

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.154	#N/A	#N/A	#N/A	#N/A



Project:	Buris Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

Buris Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																										
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics			Forest/Woodland			Pasture/Lawns			Meadows			Gravel			Impervious			Wetland/Lakes/SWMP			Average CN for Soil Type
					Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
gus	GUERIN	AB	Sand Loam	1	37	1	7.4	0.2	46	25.9	0.7	59	0	0	51	3.7	0.1	89	0	0	100	0	0	50	59.4	
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0	
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0	
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0	
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	
Totals					37	1	7.4	0.2	46	25.9	0.7	59	0	0	51	3.7	0.1	89	0	0	100	0	0	50	59.4	

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation	<input type="text" value="282"/> m
Minimum Catchment Elevation	<input type="text" value="272"/> m
Catchment length	<input type="text" value="750"/> m
Catchment Slope	<input type="text" value="1%"/>
Catchment Area	<input type="text" value="37"/> ha

Time of Concentration (Minutes)	<input type="text" value="28.13"/>
Time of Concentration (Hours)	<input type="text" value="0.47"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.31"/>

Time to Peak	<input type="text" value="0.86"/> hrs
--------------	---------------------------------------

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation	<input type="text" value="282"/> m
Minimum Catchment Elevation	<input type="text" value="272"/> m
Catchment length	<input type="text" value="750"/> m
Catchment Slope	<input type="text" value="1%"/>
Catchment Area	<input type="text" value="37"/> ha

Time of Concentration (Minutes)	<input type="text" value="77.46"/>
Time of Concentration (Hours)	<input type="text" value="1.29"/>
Time to Peak (2/3 x Time of Concentration)	<input type="text" value="0.86"/>

Initial Abstraction mm

Wetlands	<input type="text" value="12"/>
Woods	<input type="text" value="10"/>
Meadows	<input type="text" value="8"/>
Gravel	<input type="text" value="3"/>
Lawns	<input type="text" value="5"/>
Impervious	<input type="text" value="2"/>

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMP	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.146	#N/A	#N/A	#N/A	#N/A



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie

Project:	BurIs Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

BurIs Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows		Gravel			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type	
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent		CN
gus	GUERIN	AB	Sand Loam	1	17.49	1	15.74	0.9	46	1.399	0.08	59	0	0	51	0.175	0.01	89	0.175	0.01	100	0	0	50	48.01
stsl	SARGENT	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
vasl	VASEY	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
ans	ALLISTON	AB	Sand Loam	1	0	0	0	0	46	0	0	59	0	0	51	0	0	89	0	0	100	0	0	50	0
	#N/A	#N/A	#N/A	#N/A	0	0	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0	0	#N/A	0
Totals					17.49	1	15.741	0.9		1.3992	0.08		0	0	0.1749	0.01		0.1749	0.01		0	0		0	48.0

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransty-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction mm

Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2

Runoff Coefficient

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.096	#N/A	#N/A	#N/A	#N/A



C.C. Tatham & Associates Ltd.
Consulting Engineers

Collingwood Bracebridge Orillia Barrie

Project:	BurIs Creek Event Grounds
File No.:	115032
Date:	9-Apr-15
Designed By:	AR
Checked By:	ALK
Subject:	CN Calculator

BurIs Creek Event Grounds
CURVE NUMBER, INITIAL ABSTRACTION & TIME TO PEAK CALCULATIONS

CONDITIONS

Catchment Area ha

WEIGHTED CN VALUE																									
Soil Series	Soil Series	Hydrologic Soil Group	Soil Texture	Runoff Coefficient Type	Catchment Soil Characteristics		Forest/Woodland			Pasture/Lawns			Meadows			Gravel			Impervious			Wetland/Lakes/SWMF			Average CN for Soil Type
					Area	Percent	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	Area	Percent	CN	
gus	GUERIN	AB	Sand Loam	1	30.5	1	6.1	0.2	46	16.17	0.53	59	0	51	7.93	0.26	89	0.305	0.01	100	1.83	0.06	50	67.61	
stsl	SARGENT	AB	Sand Loam	1	0		0		46	0		59	0	51	0		89	0		100	0		50	0	
vsl	VASEY	AB	Sand Loam	1	0		0		46	0		59	0	51	0		89	0		100	0		50	0	
ans	ALLISTON	AB	Sand Loam	1	0		0		46	0		59	0	51	0		89	0		100	0		50	0	
	#N/A	#N/A	#N/A	#N/A	0		0		#N/A	0		#N/A	0	#N/A	0		#N/A	0		#N/A	0		#N/A	0	
Totals					30.5	1	6.1	0.2	46	16.17	0.53	59	0	51	7.93	0.26	89	0.305	0.01	100	1.83	0.06	50	67.61	

Time of Concentration Calculations

For Runoff Coefficients greater than 0.4

Bransby-Williams Formula

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Time to Peak hrs

For Runoff Coefficients less than 0.4

Airport Method

Maximum Catchment Elevation m
 Minimum Catchment Elevation m
 Catchment length m
 Catchment Slope
 Catchment Area ha

Time of Concentration (Minutes)
 Time of Concentration (Hours)
 Time to Peak (2/3 x Time of Concentration)

Initial Abstraction	6.17 mm
Wetlands	12
Woods	10
Meadows	8
Gravel	3
Lawns	5
Impervious	2
Runoff Coefficient	0.24

Landuse Type	Soil Series				
	gus	0	0	0	0
Forest/Woodland	0.08	#N/A	#N/A	#N/A	#N/A
Gravel	0.6	#N/A	#N/A	#N/A	#N/A
Pasture/Lawn	0.1	#N/A	#N/A	#N/A	#N/A
Impervious	0.95	#N/A	#N/A	#N/A	#N/A
Wetland/Lake/SWMF	0.05	#N/A	#N/A	#N/A	#N/A
Meadows	0.09	#N/A	#N/A	#N/A	#N/A
Soil Series Total	0.238	#N/A	#N/A	#N/A	#N/A

```

V V I SSSSS U U A L
V V I SS U U A A L
V V I SS U U A A A A L
V V I SS U U A A L
VV I SSSSS UUUUU A A LLLLL

OOO TTTTT TTTTT H H Y Y M M OOO TM
O O T T H H Y Y MM MM O O
O O T T H H Y M M O O
OOO T T H H Y M M OOO

```

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***** S U M M A R Y O U T P U T *****

Input filename: C:\Program Files\Visual OTTHYMO 2.2.4\voin.dat
 Output filename: I:\2015PR~1\115032~1\Design\SWM\OTTHYM~1\Proposed CHI.out
 Summary filename: I:\2015PR~1\115032~1\Design\SWM\OTTHYM~1\Proposed CHI.sum

DATE: 6/4/2015 TIME: 9:15:31 AM

USER:

COMMENTS: Proposed Condition Chicago Design Storm

 ** SIMULATION NUMBER: 1 **

W/E	COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
	START @ .00 hrs								

	READ STORM		10.0						
	[Ptot= 33.84 mm]								
	fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 2-yr Orillia.stm								
	remark: 2-Year Orillia 4-hour Chicago Storm								
*									
*	CALIB STANDHYD	0304	1 5.0	46.90	1.63	1.42	13.59	.40	.000
	[I%=20.0:S%= 2.00]								
*									
*	CALIB NASHYD	0303	1 5.0	162.73	.38	3.50	3.12	.09	.000
	[CN=56.8]								
	[N = 3.0:Tp 1.56]								
*									
*	CALIB NASHYD	0305	1 5.0	18.93	.03	4.67	3.37	.10	.000
	[CN=57.8]								
	[N = 3.0:Tp 2.55]								
*									
*	CALIB NASHYD	0201	1 5.0	71.81	.32	2.75	4.41	.13	.000
	[CN=61.6]								
	[N = 3.0:Tp 1.07]								
*									
*	CALIB NASHYD	0301	1 5.0	212.69	.38	4.67	3.37	.10	.000
	[CN=57.8]								
	[N = 3.0:Tp 2.55]								
*									
*	CALIB NASHYD	0204	1 5.0	37.00	.17	2.50	3.90	.12	.000
	[CN=59.4]								
	[N = 3.0:Tp .86]								
*									
*	CALIB NASHYD	0302	1 5.0	115.98	.41	3.17	4.17	.12	.000
	[CN=64.3]								
	[N = 3.0:Tp 1.32]								
*									
*	CALIB NASHYD	0308	1 5.0	187.19	.65	4.58	6.39	.19	.000
	[CN=75.7]								
	[N = 3.0:Tp 2.51]								
*									
*	CALIB NASHYD	0206	1 5.0	30.50	.19	2.33	5.12	.15	.000
	[CN=67.6]								
	[N = 3.0:Tp .78]								
*									
*	CALIB NASHYD	0202	1 5.0	29.42	.15	2.33	3.99	.12	.000
	[CN=59.5]								
	[N = 3.0:Tp .74]								
*									
*	CALIB NASHYD	0203	1 5.0	42.47	.11	2.92	2.67	.08	.000

```

[CN=53.7 ]
[ N = 3.0:Tp 1.12]
*
* CALIB NASHYD      0205  1  5.0  17.49   .03  3.42  1.99  .06  .000
[CN=48.0 ]
[ N = 3.0:Tp 1.44]
*
* CALIB NASHYD      0307  1  5.0  191.06   .66  4.58  6.39  .19  .000
[CN=75.7 ]
[ N = 3.0:Tp 2.51]
*
* CALIB NASHYD      0306  1  5.0  127.89   .44  4.58  6.39  .19  .000
[CN=75.7 ]
[ N = 3.0:Tp 2.51]
*
ADD [0201 + 0301]  3031  3  5.0  284.50   .58  3.58  3.63  n/a  .000
*
RESRVR [ 2 : 0204] 0312  1  5.0   37.00   .16  2.67  3.90  n/a  .000
{ST= .01 ha.m }
*
ADD [0206 + 0202]  3041  3  5.0   59.92   .34  2.33  4.57  n/a  .000
*
RESRVR [ 2 : 0203] 0314  1  5.0   42.47   .09  3.83  2.67  n/a  .000
{ST= .03 ha.m }
*
ADD [0307 + 0306]  3082  3  5.0  318.95   1.10  4.58  6.39  n/a  .000
*
ADD [3031 + 0312]  3081  3  5.0  321.50   .71  3.17  3.66  n/a  .000
*
RESRVR [ 2 : 3041] 0313  1  5.0   59.92   .26  3.08  4.56  n/a  .000
{ST= .07 ha.m }
*
ADD [0313 + 0314]  3061  3  5.0  102.39   .34  3.25  3.78  n/a  .000
*
ADD [0305 + 3081]  3045  3  5.0  340.43   .73  3.25  3.65  n/a  .000
*
ADD [3061 + 0205]  3071  3  5.0  119.88   .37  3.25  3.52  n/a  .000
*
ADD [3045 + 0302]  3044  3  5.0  456.41   1.14  3.25  3.78  n/a  .000
*
ADD [3071 + 3082]  3083  3  5.0  438.83   1.38  4.25  5.60  n/a  .000
*
ADD [0303 + 3044]  3042  3  5.0  619.14   1.52  3.33  3.61  n/a  .000
*
ADD [0308 + 3083]  3084  3  5.0  626.02   2.02  4.33  5.84  n/a  .000
*
ADD [0304 + 3042]  3043  3  5.0  666.04   1.77  3.00  4.31  n/a  .000
*

```

```

*****
** SIMULATION NUMBER: 2 **
*****

```

```

W/E COMMAND          HYD ID  DT      AREA   Qpeak Tpeak  R.V.  R.C.   Qbase
                   min      ha      cms   hrs    mm
START @ .00 hrs
-----
READ STORM          10.0
[ Ptot= 44.10 mm ]
fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 5-yr Orillia.stm
remark: 5-Year Orillia 4-hour Chicago Storm

```

```

* CALIB STANDHYD    0304  1  5.0   46.90   2.53  1.33  20.30  .46  .000
[I%=20.0:S%= 2.00]
*
* CALIB NASHYD      0303  1  5.0  162.73   .72  3.42  5.77  .13  .000
[CN=56.8 ]
[ N = 3.0:Tp 1.56]
*
* CALIB NASHYD      0305  1  5.0   18.93   .06  4.58  6.15  .14  .000
[CN=57.8 ]
[ N = 3.0:Tp 2.55]
*
* CALIB NASHYD      0201  1  5.0   71.81   .57  2.67  7.70  .17  .000
[CN=61.6 ]
[ N = 3.0:Tp 1.07]
*
* CALIB NASHYD      0301  1  5.0  212.69   .70  4.58  6.15  .14  .000
[CN=57.8 ]
[ N = 3.0:Tp 2.55]
*
* CALIB NASHYD      0204  1  5.0   37.00   .30  2.42  6.92  .16  .000
[CN=59.4 ]
[ N = 3.0:Tp .86]
*
* CALIB NASHYD      0302  1  5.0  115.98   .77  3.08  7.58  .17  .000
[CN=64.3 ]
[ N = 3.0:Tp 1.32]
*

```


*	CALIB NASHYD [CN=57.8 [N = 3.0:Tp 2.55]	0301	1	5.0	212.69	.94	4.50	8.27	.16	.000
*	CALIB NASHYD [CN=59.4 [N = 3.0:Tp .86]	0204	1	5.0	37.00	.41	2.42	9.19	.18	.000
*	CALIB NASHYD [CN=64.3 [N = 3.0:Tp 1.32]	0302	1	5.0	115.98	1.03	3.00	10.13	.20	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0308	1	5.0	187.19	1.52	4.42	14.85	.29	.000
*	CALIB NASHYD [CN=67.6 [N = 3.0:Tp .78]	0206	1	5.0	30.50	.47	2.33	11.88	.23	.000
*	CALIB NASHYD [CN=59.5 [N = 3.0:Tp .74]	0202	1	5.0	29.42	.37	2.25	9.33	.18	.000
*	CALIB NASHYD [CN=53.7 [N = 3.0:Tp 1.12]	0203	1	5.0	42.47	.29	2.83	6.85	.14	.000
*	CALIB NASHYD [CN=48.0 [N = 3.0:Tp 1.44]	0205	1	5.0	17.49	.08	3.25	5.36	.11	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0307	1	5.0	191.06	1.55	4.42	14.85	.29	.000
*	CALIB NASHYD [CN=75.7 [N = 3.0:Tp 2.51]	0306	1	5.0	127.89	1.04	4.42	14.85	.29	.000
*	ADD [0201 + 0301]	3031	3	5.0	284.50	1.41	3.50	8.74	n/a	.000
*	RESRVR [2 : 0204] {ST= .02 ha.m }	0312	1	5.0	37.00	.40	2.58	9.19	n/a	.000
*	ADD [0206 + 0202]	3041	3	5.0	59.92	.84	2.25	10.63	n/a	.000
*	RESRVR [2 : 0203] {ST= .07 ha.m }	0314	1	5.0	42.47	.23	3.67	6.85	n/a	.000
*	ADD [0307 + 0306]	3082	3	5.0	318.95	2.59	4.42	14.85	n/a	.000
*	ADD [3031 + 0312]	3081	3	5.0	321.50	1.74	3.08	8.80	n/a	.000
*	RESRVR [2 : 3041] {ST= .17 ha.m }	0313	1	5.0	59.92	.63	3.00	10.63	n/a	.000
*	ADD [0313 + 0314]	3061	3	5.0	102.39	.84	3.08	9.06	n/a	.000
*	ADD [0305 + 3081]	3045	3	5.0	340.43	1.80	3.17	8.77	n/a	.000
*	ADD [3061 + 0205]	3071	3	5.0	119.88	.92	3.17	8.52	n/a	.000
*	ADD [3045 + 0302]	3044	3	5.0	456.41	2.83	3.08	9.11	n/a	.000
*	ADD [3071 + 3082]	3083	3	5.0	438.83	3.28	4.08	13.12	n/a	.000
*	ADD [0303 + 3044]	3042	3	5.0	619.14	3.80	3.17	8.77	n/a	.000
*	ADD [0308 + 3083]	3084	3	5.0	626.02	4.78	4.17	13.64	n/a	.000
*	ADD [0304 + 3042]	3043	3	5.0	666.04	4.20	3.00	9.91	n/a	.000

** SIMULATION NUMBER: 4 **

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms

START @ .00 hrs

READ STORM 10.0

[Ptot= 58.97 mm]

fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 25-yr Orillia.stm

remark: 25-Year Orillia 4-hour Chicago Storm

*	CALIB STANDHYD	0304	1	5.0	46.90	3.88	1.33	31.14	.53	.000
---	----------------	------	---	-----	-------	------	------	-------	-----	------

[I%=20.0:S%= 2.00]											
*	*	CALIB NASHYD	0303	1	5.0	162.73	1.37	3.33	10.75	.18	.000
		[CN=56.8]								
		[N = 3.0:Tp	1.56]								
*	*	CALIB NASHYD	0305	1	5.0	18.93	.12	4.50	11.34	.19	.000
		[CN=57.8]								
		[N = 3.0:Tp	2.55]								
*	*	CALIB NASHYD	0201	1	5.0	71.81	1.03	2.67	13.67	.23	.000
		[CN=61.6]								
		[N = 3.0:Tp	1.07]								
*	*	CALIB NASHYD	0301	1	5.0	212.69	1.30	4.50	11.34	.19	.000
		[CN=57.8]								
		[N = 3.0:Tp	2.55]								
*	*	CALIB NASHYD	0204	1	5.0	37.00	.57	2.42	12.47	.21	.000
		[CN=59.4]								
		[N = 3.0:Tp	.86]								
*	*	CALIB NASHYD	0302	1	5.0	115.98	1.43	3.00	13.81	.23	.000
		[CN=64.3]								
		[N = 3.0:Tp	1.32]								
*	*	CALIB NASHYD	0308	1	5.0	187.19	2.04	4.42	19.86	.34	.000
		[CN=75.7]								
		[N = 3.0:Tp	2.51]								
*	*	CALIB NASHYD	0206	1	5.0	30.50	.65	2.25	15.97	.27	.000
		[CN=67.6]								
		[N = 3.0:Tp	.78]								
*	*	CALIB NASHYD	0202	1	5.0	29.42	.51	2.25	12.62	.21	.000
		[CN=59.5]								
		[N = 3.0:Tp	.74]								
*	*	CALIB NASHYD	0203	1	5.0	42.47	.40	2.75	9.52	.16	.000
		[CN=53.7]								
		[N = 3.0:Tp	1.12]								
*	*	CALIB NASHYD	0205	1	5.0	17.49	.11	3.25	7.55	.13	.000
		[CN=48.0]								
		[N = 3.0:Tp	1.44]								
*	*	CALIB NASHYD	0307	1	5.0	191.06	2.08	4.42	19.86	.34	.000
		[CN=75.7]								
		[N = 3.0:Tp	2.51]								
*	*	CALIB NASHYD	0306	1	5.0	127.89	1.39	4.42	19.86	.34	.000
		[CN=75.7]								
		[N = 3.0:Tp	2.51]								
*		ADD [0201 + 0301]	3031	3	5.0	284.50	1.94	3.42	11.93	n/a	.000
*		RESRVR [2 : 0204]	0312	1	5.0	37.00	.56	2.58	12.47	n/a	.000
		{ST= .03 ha.m }									
*		ADD [0206 + 0202]	3041	3	5.0	59.92	1.15	2.25	14.33	n/a	.000
*		RESRVR [2 : 0203]	0314	1	5.0	42.47	.33	3.58	9.52	n/a	.000
		{ST= .10 ha.m }									
*		ADD [0307 + 0306]	3082	3	5.0	318.95	3.47	4.42	19.86	n/a	.000
*		ADD [3031 + 0312]	3081	3	5.0	321.50	2.39	3.08	11.99	n/a	.000
*		RESRVR [2 : 3041]	0313	1	5.0	59.92	.86	2.92	14.33	n/a	.000
		{ST= .23 ha.m }									
*		ADD [0313 + 0314]	3061	3	5.0	102.39	1.16	3.08	12.33	n/a	.000
*		ADD [0305 + 3081]	3045	3	5.0	340.43	2.47	3.08	11.95	n/a	.000
*		ADD [3061 + 0205]	3071	3	5.0	119.88	1.27	3.08	11.63	n/a	.000
*		ADD [3045 + 0302]	3044	3	5.0	456.41	3.90	3.08	12.42	n/a	.000
*		ADD [3071 + 3082]	3083	3	5.0	438.83	4.44	4.00	17.61	n/a	.000
*		ADD [0303 + 3044]	3042	3	5.0	619.14	5.25	3.17	11.98	n/a	.000
*		ADD [0308 + 3083]	3084	3	5.0	626.02	6.44	4.08	18.28	n/a	.000
*		ADD [0304 + 3042]	3043	3	5.0	666.04	5.72	3.00	13.33	n/a	.000

** SIMULATION NUMBER: 5 **

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms
	START @ .00 hrs									

	READ STORM			10.0						
	[Ptot= 65.52 mm]									
	fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 50-yr Orillia.stm									
	remark: 50-Year Orillia 4-hour Chicago Storm									
*										
*	CALIB STANDHYD	0304	1	5.0	46.90	5.22	1.50	36.22	.55	.000
	[I%=20.0:S%= 2.00]									
*										
*	CALIB NASHYD	0303	1	5.0	162.73	1.71	3.33	13.32	.20	.000
	[CN=56.8]									
	[N = 3.0:Tp 1.56]									
*										
*	CALIB NASHYD	0305	1	5.0	18.93	.14	4.50	13.99	.21	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*										
*	CALIB NASHYD	0201	1	5.0	71.81	1.27	2.67	16.68	.25	.000
	[CN=61.6]									
	[N = 3.0:Tp 1.07]									
*										
*	CALIB NASHYD	0301	1	5.0	212.69	1.61	4.50	13.99	.21	.000
	[CN=57.8]									
	[N = 3.0:Tp 2.55]									
*										
*	CALIB NASHYD	0204	1	5.0	37.00	.70	2.42	15.28	.23	.000
	[CN=59.4]									
	[N = 3.0:Tp .86]									
*										
*	CALIB NASHYD	0302	1	5.0	115.98	1.77	3.00	16.96	.26	.000
	[CN=64.3]									
	[N = 3.0:Tp 1.32]									
*										
*	CALIB NASHYD	0308	1	5.0	187.19	2.48	4.33	24.05	.37	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0206	1	5.0	30.50	.80	2.25	19.45	.30	.000
	[CN=67.6]									
	[N = 3.0:Tp .78]									
*										
*	CALIB NASHYD	0202	1	5.0	29.42	.63	2.25	15.46	.24	.000
	[CN=59.5]									
	[N = 3.0:Tp .74]									
*										
*	CALIB NASHYD	0203	1	5.0	42.47	.51	2.75	11.85	.18	.000
	[CN=53.7]									
	[N = 3.0:Tp 1.12]									
*										
*	CALIB NASHYD	0205	1	5.0	17.49	.14	3.17	9.49	.14	.000
	[CN=48.0]									
	[N = 3.0:Tp 1.44]									
*										
*	CALIB NASHYD	0307	1	5.0	191.06	2.53	4.33	24.05	.37	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0306	1	5.0	127.89	1.69	4.33	24.05	.37	.000
	[CN=75.7]									
	[N = 3.0:Tp 2.51]									
*										
*	ADD [0201 + 0301]	3031	3	5.0	284.50	2.39	3.42	14.67	n/a	.000
*										
*	RESRVR [2 : 0204]	0312	1	5.0	37.00	.69	2.58	15.28	n/a	.000
	{ST= .03 ha.m }									
*										
*	ADD [0206 + 0202]	3041	3	5.0	59.92	1.43	2.25	17.49	n/a	.000
*										
*	RESRVR [2 : 0203]	0314	1	5.0	42.47	.41	3.58	11.85	n/a	.000
	{ST= .12 ha.m }									
*										
*	ADD [0307 + 0306]	3082	3	5.0	318.95	4.22	4.33	24.05	n/a	.000
*										
*	ADD [3031 + 0312]	3081	3	5.0	321.50	2.95	3.00	14.74	n/a	.000
*										
*	RESRVR [2 : 3041]	0313	1	5.0	59.92	1.06	2.92	17.49	n/a	.000
	{ST= .28 ha.m }									
*										
*	ADD [0313 + 0314]	3061	3	5.0	102.39	1.43	3.08	15.15	n/a	.000
*										
*	ADD [0305 + 3081]	3045	3	5.0	340.43	3.05	3.08	14.70	n/a	.000
*										
*	ADD [3061 + 0205]	3071	3	5.0	119.88	1.57	3.08	14.32	n/a	.000

```

* ADD [3045 + 0302] 3044 3 5.0 456.41 4.82 3.00 15.28 n/a .000
* ADD [3071 + 3082] 3083 3 5.0 438.83 5.41 3.92 21.40 n/a .000
* ADD [0303 + 3044] 3042 3 5.0 619.14 6.50 3.08 14.76 n/a .000
* ADD [0308 + 3083] 3084 3 5.0 626.02 7.85 4.08 22.19 n/a .000
* ADD [0304 + 3042] 3043 3 5.0 666.04 7.01 3.00 16.27 n/a .000

```

```

*****
** SIMULATION NUMBER: 6 **
*****

```

```

W/E COMMAND          HYD ID  DT    AREA  Qpeak Tpeak  R.V.  R.C.  Qbase
                   min     ha    cms   hrs   mm
START @ .00 hrs
-----
READ STORM          10.0
[ Ptot= 71.71 mm ]
fname : I:\2015 Projects\115032 - Burls Creek\Design\SWM\OTTHYMO Model\storms\Orillia\CHI 100-yr Orillia.stm
remark: 100-Year Orillia 4-hour Chicago Storm

```

```

* CALIB STANDHYD    0304 1 5.0  46.90  6.10  1.50  41.16  .57  .000
  [I%=20.0:S%= 2.00]
* CALIB NASHYD      0303 1 5.0 162.73  2.05  3.33  15.93  .22  .000
  [CN=56.8          ]
  [ N = 3.0:Tp 1.56]
* CALIB NASHYD      0305 1 5.0  18.93  .17  4.42  16.69  .23  .000
  [CN=57.8          ]
  [ N = 3.0:Tp 2.55]
* CALIB NASHYD      0201 1 5.0  71.81  1.51  2.67  19.72  .27  .000
  [CN=61.6          ]
  [ N = 3.0:Tp 1.07]
* CALIB NASHYD      0301 1 5.0 212.69  1.92  4.42  16.69  .23  .000
  [CN=57.8          ]
  [ N = 3.0:Tp 2.55]
* CALIB NASHYD      0204 1 5.0  37.00  .84  2.42  18.14  .25  .000
  [CN=59.4          ]
  [ N = 3.0:Tp .86]
* CALIB NASHYD      0302 1 5.0 115.98  2.11  3.00  20.14  .28  .000
  [CN=64.3          ]
  [ N = 3.0:Tp 1.32]
* CALIB NASHYD      0308 1 5.0 187.19  2.91  4.33  28.22  .39  .000
  [CN=75.7          ]
  [ N = 3.0:Tp 2.51]
* CALIB NASHYD      0206 1 5.0  30.50  .95  2.25  22.94  .32  .000
  [CN=67.6          ]
  [ N = 3.0:Tp .78]
* CALIB NASHYD      0202 1 5.0  29.42  .75  2.25  18.32  .26  .000
  [CN=59.5          ]
  [ N = 3.0:Tp .74]
* CALIB NASHYD      0203 1 5.0  42.47  .61  2.75  14.24  .20  .000
  [CN=53.7          ]
  [ N = 3.0:Tp 1.12]
* CALIB NASHYD      0205 1 5.0  17.49  .17  3.17  11.49  .16  .000
  [CN=48.0          ]
  [ N = 3.0:Tp 1.44]
* CALIB NASHYD      0307 1 5.0 191.06  2.97  4.33  28.22  .39  .000
  [CN=75.7          ]
  [ N = 3.0:Tp 2.51]
* CALIB NASHYD      0306 1 5.0 127.89  1.99  4.33  28.22  .39  .000
  [CN=75.7          ]
  [ N = 3.0:Tp 2.51]
* ADD [0201 + 0301] 3031 3 5.0 284.50  2.85  3.42  17.46 n/a .000
* RESRVR [ 2 : 0204] 0312 1 5.0  37.00  .82  2.50  18.14 n/a .000
  {ST= .04 ha.m }
* ADD [0206 + 0202] 3041 3 5.0  59.92  1.70  2.25  20.67 n/a .000
* RESRVR [ 2 : 0203] 0314 1 5.0  42.47  .49  3.58  14.24 n/a .000
  {ST= .15 ha.m }

```



```

* CALIB NASHYD          0306  1  5.0  127.89   5.83 10.42 128.77  .67   .000
  [CN=75.7              ]
  [ N = 3.0:Tp 2.51]
*
* ADD [0201 + 0301]    3031  3  5.0  284.50   9.70  9.92  95.31  n/a   .000
*
* RESRVR [ 2 : 0204]  0312  1  5.0   37.00   .94 11.67  97.12  n/a   .000
  {ST= .94 ha.m }
*
* ADD [0206 + 0202]    3041  3  5.0   59.92   3.37  7.50 105.47  n/a   .000
*
* RESRVR [ 2 : 0203]  0314  1  5.0   42.47   .96 12.08  84.50  n/a   .000
  {ST= 1.24 ha.m }
*
* ADD [0307 + 0306]    3082  3  5.0  318.95  14.53 10.42 128.77  n/a   .000
*
* ADD [3031 + 0312]    3081  3  5.0  321.50  10.63  9.92  95.52  n/a   .000
*
* RESRVR [ 2 : 3041]  0313  1  5.0   59.92   1.46 11.83 105.47  n/a   .000
  {ST= 2.22 ha.m }
*
* ADD [0313 + 0314]    3061  3  5.0  102.39   2.42 12.08  96.77  n/a   .000
*
* ADD [0305 + 3081]    3045  3  5.0  340.43  11.24 10.00  95.38  n/a   .000
*
* ADD [3061 + 0205]    3071  3  5.0  119.88   2.89 10.17  93.37  n/a   .000
*
* ADD [3045 + 0302]    3044  3  5.0  456.41  16.40  9.58  97.94  n/a   .000
*
* ADD [3071 + 3082]    3083  3  5.0  438.83  17.42 10.42 119.10  n/a   .000
*
* ADD [0303 + 3044]    3042  3  5.0  619.14  22.68  9.58  96.05  n/a   .000
*
* ADD [0308 + 3083]    3084  3  5.0  626.02  25.94 10.42 121.99  n/a   .000
*
* ADD [0304 + 3042]    3043  3  5.0  666.04  24.91  9.17  99.87  n/a   .000
*

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FINISH
=====

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* CALIB NASHYD      0202  1  5.0   29.42    .19 12.83   8.17  .17   .000
  [CN=59.5        ]
  [ N = 3.0:Tp   .74]
*
* CALIB NASHYD      0206  1  5.0   30.50    .25 12.83  10.43  .22   .000
  [CN=67.6        ]
  [ N = 3.0:Tp   .78]
*
* CALIB NASHYD      0308  1  5.0  187.19    .89 15.17  13.06  .28   .000
  [CN=75.7        ]
  [ N = 3.0:Tp  2.51]
*
RESRVR [ 2 : 0204] 0312  1  5.0   37.00    .21 13.08   8.04  n/a   .000
{ST=   .01 ha.m }
*
ADD [0301 + 0201] 3031  3  5.0  284.50    .78 14.33   7.63  n/a   .000
*
ADD [0306 + 0307] 3082  3  5.0  318.95    1.52 15.17  13.06  n/a   .000
*
RESRVR [ 2 : 0203] 0314  1  5.0   42.47    .12 14.25   5.92  n/a   .000
{ST=   .04 ha.m }
*
ADD [0202 + 0206] 3041  3  5.0   59.92    .43 12.83   9.32  n/a   .000
*
ADD [0312 + 3031] 3081  3  5.0  321.50    .95 13.50   7.68  n/a   .000
*
RESRVR [ 2 : 3041] 0313  1  5.0   59.92    .34 13.50   9.32  n/a   .000
{ST=   .09 ha.m }
*
ADD [3081 + 0305] 3045  3  5.0  340.43    .98 13.58   7.65  n/a   .000
*
ADD [0314 + 0313] 3061  3  5.0  102.39    .45 13.58   7.91  n/a   .000
*
ADD [0302 + 3045] 3044  3  5.0  456.41    1.53 13.58   7.95  n/a   .000
*
ADD [0205 + 3061] 3071  3  5.0  119.88    .49 13.58   7.43  n/a   .000
*
ADD [3044 + 0303] 3042  3  5.0  619.14    2.05 13.67   7.64  n/a   .000
*
ADD [3082 + 3071] 3083  3  5.0  438.83    1.88 14.75  11.52  n/a   .000
*
ADD [3042 + 0304] 3043  3  5.0  666.04    2.40 13.08   8.69  n/a   .000
*
ADD [3083 + 0308] 3084  3  5.0  626.02    2.76 14.92  11.98  n/a   .000

```

```

*****
** SIMULATION NUMBER: 2 **
*****

```

```

W/E COMMAND          HYD ID  DT   AREA   Qpeak Tpeak   R.V. R.C.   Qbase
                   min   ha    cms   hrs    mm
START @   .00 hrs
-----
MASS STORM          20.0
[ Ptot= 61.80 mm ]
*
** CALIB NASHYD      0302  1  5.0  115.98    .98 13.50  15.14  .25   .000
  [CN=64.3        ]
  [ N = 3.0:Tp  1.32]
*
** CALIB NASHYD      0204  1  5.0   37.00    .37 12.92  13.66  .22   .000
  [CN=59.4        ]
  [ N = 3.0:Tp   .86]
*
** CALIB NASHYD      0301  1  5.0  212.69    .94 15.25  12.46  .20   .000
  [CN=57.8        ]
  [ N = 3.0:Tp  2.55]
*
** CALIB NASHYD      0201  1  5.0   71.81    .69 13.17  14.95  .24   .000
  [CN=61.6        ]
  [ N = 3.0:Tp  1.07]
*
** CALIB NASHYD      0305  1  5.0   18.93    .08 15.25  12.46  .20   .000
  [CN=57.8        ]
  [ N = 3.0:Tp  2.55]
*
** CALIB NASHYD      0303  1  5.0  162.73    .94 13.83  11.84  .19   .000
  [CN=56.8        ]
  [ N = 3.0:Tp  1.56]
*
* CALIB STANDHYD     0304  1  5.0   46.90    1.84 12.08  33.32  .54   .000
  [I%=20.0:S%= 2.00]
*
* CALIB NASHYD      0306  1  5.0  127.89    1.03 15.08  21.64  .35   .000
  [CN=75.7        ]
  [ N = 3.0:Tp  2.51]

```


**	CALIB NASHYD	0303	1	5.0	162.73	1.26	13.75	15.75	.22	.000
	[CN=56.8									
	[N = 3.0:Tp 1.56]									
*										
*	CALIB STANDHYD	0304	1	5.0	46.90	2.31	12.08	40.83	.57	.000
	[I%=20.0:S%= 2.00]									
*										
*	CALIB NASHYD	0306	1	5.0	127.89	1.34	15.00	27.94	.39	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0307	1	5.0	191.06	2.01	15.00	27.94	.39	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
*	CALIB NASHYD	0205	1	5.0	17.49	.10	13.67	11.35	.16	.000
	[CN=48.0									
	[N = 3.0:Tp 1.44]									
*										
*	CALIB NASHYD	0203	1	5.0	42.47	.37	13.25	14.07	.20	.000
	[CN=53.7									
	[N = 3.0:Tp 1.12]									
*										
*	CALIB NASHYD	0202	1	5.0	29.42	.43	12.75	18.13	.25	.000
	[CN=59.5									
	[N = 3.0:Tp .74]									
*										
*	CALIB NASHYD	0206	1	5.0	30.50	.55	12.83	22.70	.32	.000
	[CN=67.6									
	[N = 3.0:Tp .78]									
*										
*	CALIB NASHYD	0308	1	5.0	187.19	1.97	15.00	27.94	.39	.000
	[CN=75.7									
	[N = 3.0:Tp 2.51]									
*										
	RESRVR [2 : 0204]	0312	1	5.0	37.00	.49	13.08	17.94	n/a	.000
	{ST= .02 ha.m }									
*										
	ADD [0301 + 0201]	3031	3	5.0	284.50	1.81	14.25	17.27	n/a	.000
*										
	ADD [0306 + 0307]	3082	3	5.0	318.95	3.35	15.00	27.94	n/a	.000
*										
	RESRVR [2 : 0203]	0314	1	5.0	42.47	.30	14.08	14.07	n/a	.000
	{ST= .09 ha.m }									
*										
	ADD [0202 + 0206]	3041	3	5.0	59.92	.98	12.83	20.46	n/a	.000
*										
	ADD [0312 + 3031]	3081	3	5.0	321.50	2.20	13.50	17.35	n/a	.000
*										
	RESRVR [2 : 3041]	0313	1	5.0	59.92	.77	13.42	20.45	n/a	.000
	{ST= .20 ha.m }									
*										
	ADD [3081 + 0305]	3045	3	5.0	340.43	2.28	13.58	17.30	n/a	.000
*										
	ADD [0314 + 0313]	3061	3	5.0	102.39	1.05	13.58	17.81	n/a	.000
*										
	ADD [0302 + 3045]	3044	3	5.0	456.41	3.59	13.50	17.97	n/a	.000
*										
	ADD [0205 + 3061]	3071	3	5.0	119.88	1.15	13.58	16.87	n/a	.000
*										
	ADD [3044 + 0303]	3042	3	5.0	619.14	4.84	13.58	17.38	n/a	.000
*										
	ADD [3082 + 3071]	3083	3	5.0	438.83	4.23	14.58	24.91	n/a	.000
*										
	ADD [3042 + 0304]	3043	3	5.0	666.04	5.39	13.17	19.04	n/a	.000
*										
	ADD [3083 + 0308]	3084	3	5.0	626.02	6.17	14.75	25.82	n/a	.000
*										

** SIMULATION NUMBER: 4 **

W/E	COMMAND	HYD	ID	DT	AREA	Qpeak	Tpeak	R.V.	R.C.	Qbase
				min	ha	cms	hrs	mm		cms
	START @ .00 hrs									

	MASS STORM			20.0						
	[Ptot= 83.30 mm]									
*										
**	CALIB NASHYD	0302	1	5.0	115.98	1.76	13.42	26.56	.32	.000
	[CN=64.3									
	[N = 3.0:Tp 1.32]									
*										
**	CALIB NASHYD	0204	1	5.0	37.00	.66	12.92	23.92	.29	.000
	[CN=59.4									
	[N = 3.0:Tp .86]									
*										
**	CALIB NASHYD	0301	1	5.0	212.69	1.71	15.17	22.19	.27	.000

	[CN=57.8 [N = 3.0:Tp 2.55]									
**	CALIB NASHYD	0201	1	5.0	71.81	1.22	13.17	25.85	.31	.000
	[CN=61.6 [N = 3.0:Tp 1.07]									
**	CALIB NASHYD	0305	1	5.0	18.93	.15	15.17	22.19	.27	.000
	[CN=57.8 [N = 3.0:Tp 2.55]									
**	CALIB NASHYD	0303	1	5.0	162.73	1.73	13.75	21.26	.26	.000
	[CN=56.8 [N = 3.0:Tp 1.56]									
*	CALIB STANDHYD	0304	1	5.0	46.90	2.95	12.08	50.69	.61	.000
	[I%=20.0:S%= 2.00]									
*	CALIB NASHYD	0306	1	5.0	127.89	1.77	15.00	36.45	.44	.000
	[CN=75.7 [N = 3.0:Tp 2.51]									
*	CALIB NASHYD	0307	1	5.0	191.06	2.64	15.00	36.45	.44	.000
	[CN=75.7 [N = 3.0:Tp 2.51]									
*	CALIB NASHYD	0205	1	5.0	17.49	.14	13.58	15.63	.19	.000
	[CN=48.0 [N = 3.0:Tp 1.44]									
*	CALIB NASHYD	0203	1	5.0	42.47	.51	13.25	19.13	.23	.000
	[CN=53.7 [N = 3.0:Tp 1.12]									
*	CALIB NASHYD	0202	1	5.0	29.42	.58	12.75	24.13	.29	.000
	[CN=59.5 [N = 3.0:Tp .74]									
*	CALIB NASHYD	0206	1	5.0	30.50	.73	12.83	29.91	.36	.000
	[CN=67.6 [N = 3.0:Tp .78]									
*	CALIB NASHYD	0308	1	5.0	187.19	2.59	15.00	36.45	.44	.000
	[CN=75.7 [N = 3.0:Tp 2.51]									
	RESRVR [2 : 0204	0312	1	5.0	37.00	.65	13.08	23.92	n/a	.000
	{ST= .03 ha.m }									
	ADD [0301 + 0201]	3031	3	5.0	284.50	2.45	14.17	23.11	n/a	.000
	ADD [0306 + 0307]	3082	3	5.0	318.95	4.41	15.00	36.45	n/a	.000
	RESRVR [2 : 0203	0314	1	5.0	42.47	.41	14.08	19.13	n/a	.000
	{ST= .12 ha.m }									
	ADD [0202 + 0206]	3041	3	5.0	59.92	1.31	12.75	27.08	n/a	.000
	ADD [0312 + 3031]	3081	3	5.0	321.50	2.98	13.50	23.21	n/a	.000
	RESRVR [2 : 3041	0313	1	5.0	59.92	1.03	13.42	27.08	n/a	.000
	{ST= .27 ha.m }									
	ADD [3081 + 0305]	3045	3	5.0	340.43	3.09	13.50	23.15	n/a	.000
	ADD [0314 + 0313]	3061	3	5.0	102.39	1.41	13.58	23.78	n/a	.000
	ADD [0302 + 3045]	3044	3	5.0	456.41	4.85	13.50	24.02	n/a	.000
	ADD [0205 + 3061]	3071	3	5.0	119.88	1.55	13.58	22.59	n/a	.000
	ADD [3044 + 0303]	3042	3	5.0	619.14	6.55	13.58	23.29	n/a	.000
	ADD [3082 + 3071]	3083	3	5.0	438.83	5.60	14.58	32.66	n/a	.000
	ADD [3042 + 0304]	3043	3	5.0	666.04	7.20	13.17	25.22	n/a	.000
	ADD [3083 + 0308]	3084	3	5.0	626.02	8.16	14.67	33.79	n/a	.000

** SIMULATION NUMBER: 5 **

W/E COMMAND	HYD ID	DT min	AREA ha	Qpeak cms	Tpeak hrs	R.V. mm	R.C.	Qbase cms
START @ .00 hrs								

MASS STORM		20.0						

```

[ Ptot= 92.20 mm ]
*
** CALIB NASHYD      0302  1  5.0  115.98    2.13 13.42  31.84  .35   .000
   [CN=64.3        ]
   [ N = 3.0:Tp  1.32]
*
** CALIB NASHYD      0204  1  5.0   37.00     .80 12.92  28.71  .31   .000
   [CN=59.4        ]
   [ N = 3.0:Tp   .86]
*
** CALIB NASHYD      0301  1  5.0  212.69    2.07 15.08  26.77  .29   .000
   [CN=57.8        ]
   [ N = 3.0:Tp  2.55]
*
** CALIB NASHYD      0201  1  5.0   71.81    1.47 13.17  30.90  .34   .000
   [CN=61.6        ]
   [ N = 3.0:Tp  1.07]
*
** CALIB NASHYD      0305  1  5.0   18.93     .18 15.08  26.77  .29   .000
   [CN=57.8        ]
   [ N = 3.0:Tp  2.55]
*
** CALIB NASHYD      0303  1  5.0  162.73    2.10 13.75  25.71  .28   .000
   [CN=56.8        ]
   [ N = 3.0:Tp  1.56]
*
* CALIB STANDHYD     0304  1  5.0   46.90    3.64 12.08  58.23  .63   .000
   [I%=20.0:S%=  2.00]
*
* CALIB NASHYD      0306  1  5.0  127.89    2.10 14.92  43.08  .47   .000
   [CN=75.7        ]
   [ N = 3.0:Tp  2.51]
*
* CALIB NASHYD      0307  1  5.0  191.06    3.14 14.92  43.08  .47   .000
   [CN=75.7        ]
   [ N = 3.0:Tp  2.51]
*
* CALIB NASHYD      0205  1  5.0   17.49     .17 13.58  19.13  .21   .000
   [CN=48.0        ]
   [ N = 3.0:Tp  1.44]
*
* CALIB NASHYD      0203  1  5.0   42.47     .62 13.25  23.24  .25   .000
   [CN=53.7        ]
   [ N = 3.0:Tp  1.12]
*
* CALIB NASHYD      0202  1  5.0   29.42     .70 12.75  28.95  .31   .000
   [CN=59.5        ]
   [ N = 3.0:Tp   .74]
*
* CALIB NASHYD      0206  1  5.0   30.50     .88 12.83  35.62  .39   .000
   [CN=67.6        ]
   [ N = 3.0:Tp   .78]
*
* CALIB NASHYD      0308  1  5.0  187.19    3.07 14.92  43.08  .47   .000
   [CN=75.7        ]
   [ N = 3.0:Tp  2.51]
*
RESRVR [ 2 : 0204] 0312  1  5.0   37.00     .79 13.08  28.71  n/a   .000
{ST=   .04 ha.m }
*
ADD [0301 + 0201] 3031  3  5.0  284.50    2.96 14.17  27.81  n/a   .000
*
ADD [0306 + 0307] 3082  3  5.0  318.95    5.24 14.92  43.08  n/a   .000
*
RESRVR [ 2 : 0203] 0314  1  5.0   42.47     .51 14.08  23.24  n/a   .000
{ST=   .15 ha.m }
*
ADD [0202 + 0206] 3041  3  5.0   59.92    1.57 12.75  32.34  n/a   .000
*
ADD [0312 + 3031] 3081  3  5.0  321.50    3.60 13.50  27.92  n/a   .000
*
RESRVR [ 2 : 3041] 0313  1  5.0   59.92    1.24 13.42  32.34  n/a   .000
{ST=   .33 ha.m }
*
ADD [3081 + 0305] 3045  3  5.0  340.43    3.74 13.50  27.85  n/a   .000
*
ADD [0314 + 0313] 3061  3  5.0  102.39    1.70 13.50  28.57  n/a   .000
*
ADD [0302 + 3045] 3044  3  5.0  456.41    5.86 13.50  28.87  n/a   .000
*
ADD [0205 + 3061] 3071  3  5.0  119.88    1.87 13.58  27.19  n/a   .000
*
ADD [3044 + 0303] 3042  3  5.0  619.14    7.93 13.58  28.04  n/a   .000
*
ADD [3082 + 3071] 3083  3  5.0  438.83    6.69 14.50  38.74  n/a   .000
*
ADD [3042 + 0304] 3043  3  5.0  666.04    8.60 13.17  30.16  n/a   .000
*
ADD [3083 + 0308] 3084  3  5.0  626.02    9.73 14.67  40.04  n/a   .000

```


*
ADD [0302 + 3045] 3044 3 5.0 456.41 6.93 13.50 33.99 n/a .000
*
ADD [0205 + 3061] 3071 3 5.0 119.88 2.22 13.50 32.06 n/a .000
*
ADD [3044 + 0303] 3042 3 5.0 619.14 9.40 13.50 33.06 n/a .000
*
ADD [3082 + 3071] 3083 3 5.0 438.83 7.82 14.50 45.06 n/a .000
*
ADD [3042 + 0304] 3043 3 5.0 666.04 10.14 13.17 35.37 n/a .000
*
ADD [3083 + 0308] 3084 3 5.0 626.02 11.36 14.58 46.52 n/a .000
*

FINISH

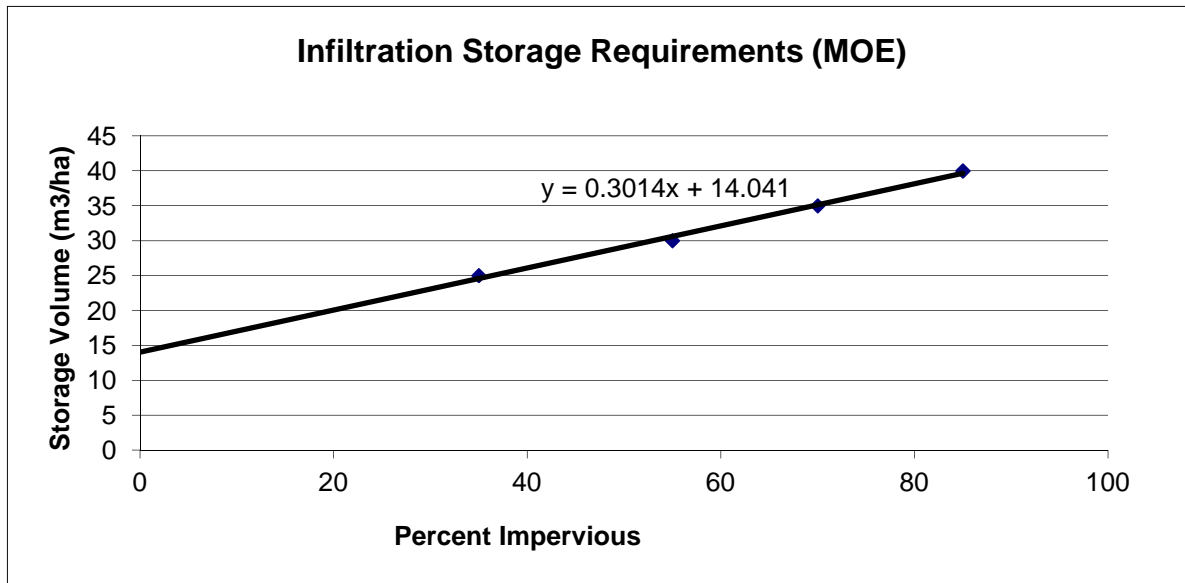
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**APPENDIX C:
PRELIMINARY DESIGN CALCULATIONS**

MOE Water Quality Storage Volumes

Table 3.1 Values

% imp	storage (m³/ha)
35	25
55	30
70	35
85	40



Contributing Areas

		Area (ha)	Proposed Gravel (%)	Proposed Impervious (%)	Proposed Combined (%)	Storage Volume (m³/ha)	Storage Volume (m³)
Catchment	201	71.81	4	1	5	15.5	1116.5
Catchment	203	42.47	12	0	12	17.7	749.9
Catchment	204	37	5	0	5	15.5	575.3
Catchment	206	30.5	10	0	10	17.1	520.2
TOTAL AREA		181.78	7.1	0.4	7.5	65.8	2961.9

Catchment	Swale Length Required	Swale Length Provided	Storage Volume Required	Controlling Factor	Storage Volume Provided	Area	Bottom Width	Top Width	Depth
201	992	1065	1116	Quality	1198	1.125	0.75	3.75	0.5
203	1620	1725	1822	Quantity	1941				
204	511	700	575	Quality	788				
206	3422	3640	3850	Quantity	4095				
Total	6545	7130	7363		8021				

Catchment	201	202	203	204	206
Swale Sections	640	530	790	700	750
	350	180	740		230
	75	200	120		390
		280	75		210
		310			140
		310			80
					180
					100
					250
					-500 MTO Swale
Total Swale Length	1065	1810	1725	700	1830
					3640 202+206

Culvert Calculator Report

A-A

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	100.80 m	Headwater Depth/Height	2.62
Computed Headwater Elev:	100.80 m	Discharge	0.2172 m ³ /s
Inlet Control HW Elev.	100.57 m	Tailwater Elevation	99.91 m
Outlet Control HW Elev.	100.80 m	Control Type	Outlet Control

Grades			
Upstream Invert	100.00 m	Downstream Invert	99.91 m
Length	10.00 m	Constructed Slope	0.009000 m/m

Hydraulic Profile			
Profile	CompositeM2PressureProfile	Depth, Downstream	0.25 m
Slope Type	Mild	Normal Depth	N/A m
Flow Regime	Subcritical	Critical Depth	0.25 m
Velocity Downstream	1.67 m/s	Critical Slope	0.038432 m/m

Section			
Section Shape	Circular	Mannings Coefficient	0.024
Section Material	CMP	Span	0.30 m
Section Size	300 mm	Rise	0.30 m
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	100.80 m	Upstream Velocity Head	0.11 m
Ke	0.90	Entrance Loss	0.10 m

Inlet Control Properties			
Inlet Control HW Elev.	100.57 m	Flow Control	N/A
Inlet Type	Projecting	Area Full	0.1 m ²
K	0.03400	HDS 5 Chart	2
M	1.50000	HDS 5 Scale	3
C	0.05530	Equation Form	1
Y	0.54000		

Worksheet for Swale at 1%

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.01000	m/m
Normal Depth	0.50	m
Left Side Slope	3.00	m/m (H:V)
Right Side Slope	3.00	m/m (H:V)
Bottom Width	0.75	m

Results

Discharge	1.63	m ³ /s
Flow Area	1.13	m ²
Wetted Perimeter	3.91	m
Hydraulic Radius	0.29	m
Top Width	3.75	m
Critical Depth	0.46	m
Critical Slope	0.01426	m/m
Velocity	1.45	m/s
Velocity Head	0.11	m
Specific Energy	0.61	m
Froude Number	0.85	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.50	m
Critical Depth	0.46	m
Channel Slope	0.01000	m/m

Worksheet for Swale at 1%

GVF Output Data

Critical Slope 0.01426 m/m

Worksheet for Swale at 0.5%

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.00500	m/m
Normal Depth	0.50	m
Left Side Slope	3.00	m/m (H:V)
Right Side Slope	3.00	m/m (H:V)
Bottom Width	0.75	m

Results

Discharge	1.16	m ³ /s
Flow Area	1.13	m ²
Wetted Perimeter	3.91	m
Hydraulic Radius	0.29	m
Top Width	3.75	m
Critical Depth	0.39	m
Critical Slope	0.01493	m/m
Velocity	1.03	m/s
Velocity Head	0.05	m
Specific Energy	0.55	m
Froude Number	0.60	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	m
Length	0.00	m
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	m
Profile Description		
Profile Headloss	0.00	m
Downstream Velocity	Infinity	m/s
Upstream Velocity	Infinity	m/s
Normal Depth	0.50	m
Critical Depth	0.39	m
Channel Slope	0.00500	m/m

Worksheet for Swale at 0.5%

GVF Output Data

Critical Slope 0.01493 m/m