Functional Servicing & Stormwater Management Report Overhead Bridge Road 6 Lots Township of Tiny

File 20-644 December 2020

Prepared by

WMI & Associates Limited 119 Collier Street, Barrie Ontario L4M 1H5



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1.0 Introduction

1.1 General

WMI & Associates Ltd. has been retained by Charlebois Properties Inc. to prepare a Functional Servicing and Stormwater Management Report for the proposed Overhead Bridge Road 6 Lots, located in the Township of Tiny, County of Simcoe.

The proposed development is located on Overhead Bridge Road (formerly County Road 61) to the west of the Town of Penetanguishene. The Whip-poor-will Development is located to the west, with the Copeland Creek developments to the north. The proposed site location is a parcel of land between 584 and 564 Overhead Bridge Road. This development comprises 5.6ha and 6 residential lots. The property is legally referred to as Part of Lot 9, Concession 12 in the Township of Tiny, County of Simcoe.

The designs described herein are based on a Legal Survey prepared by Raikes (prepared November 2020), and the topographic ground information obtained from First Base Solutions.

The engineering analysis and design outlined in this report conforms with the following:

- Township of Tiny Engineering Standards (April 2003).
- Ministry of Environment (MOE) Stormwater Management Practices Planning and Design Manual (2003).
- MOE and MNR Best Management Practices Manual (1991).
- Hydrogeological Assessment Submissions Conservation Authority Guidelines for Development Applications (June, 2013).
- South Georgian Bay Lake Simcoe Source Protection Region, Approved South Georgian Bay Lake Simcoe Source Protection Plan (January 26, 2015, Amended February 15, 2018).
- Low Impact Development Stormwater Management Planning And Design Guide Version 1.0, CVCA & TRCA (2010).
- Ontario Building Code (Sept. 14, 2012 and current addendums).

1.2 Study Purpose and Context

This report presents an investigation of existing storm drainage infrastructure and drainage patterns, and a design of proposed storm drainage systems to support the full build out of the Overhead Bridge Road 6 Lots development.

This report intends to demonstrate how the potable water supply, sewage disposal as well as the storm drainage and quality controls will be accommodated within the development and fit within the context of existing municipal infrastructure. Designs presented herein are in accordance with the Township of Tiny and Ontario Ministry of the Environment Conservation and Parks (MECP) design guidelines and regulations.

2.0 Site Servicing

2.1 Servicing Options/Feasibility Overview

The subject property is located in a privately-serviced rural area. This area of the Township is not close to either full municipal or private sewage treatment systems. The southern portion of the Whip-Poor-Will Development does operate a drinking water system comprised of one pumping station, two ground water wells and one storage reservoir. Given the potential significant cost to connect and upgrade the system it is cost prohibitive for 6 Lots. Given the significant distances and the inefficiency to connect to any existing municipal system it was concluded that this site is best developed using individual on-site water services and individual on-site sewage systems. The proposed servicing and overall feasibility of other various servicing options is discussed in the water servicing and sewage sections provided below.

In order to support the functionality of the potable water and sewage disposal, Wilson Associates completed a Hydrogeological Assessment which is included in **Appendix C.**

2.2 Water Servicing

In order to demonstrate an adequate potable water supply is available, a hydrogeologic evaluation was undertaken by Wilson Associates Ltd. The Hydrogeologic Assessment Report summarizes as follows:

"The average reported well within about 500 metres of the proposed development is of drilled construction, completed in the intermediate overburden to a depth of 57.2 metres and yields 78 litres of fresh-quality water per minute over an average period of 4.5 hours. This average yield significantly exceeds the maximum water demand of a normal four bedroom home specified by the MECP (i.e. 18L/min without inline storage). Overall groundwater conditions are very favorable for domestic water requirements. The high average well yield in the vicinity of the site is consistent with an aquifer setting that is more than capable of supplying domestic water demand with limited risk of adverse interference on the large lots proposed

Based on historical and on-going water quality analytical data from the nearby Whippoorwill wells, which are completed in the same overburden aquifer in which the on-site wells are likely to be completed, bacteriological and chemical quality of water from properly-constructed on-site drilled wells will be acceptable."

In summary, the site can be adequately supplied with water via individual drilled wells.

2.3 Sewage Disposal

The subject area and surrounding lands are not currently supplied with municipal or private communal sanitary sewage services. There are no municipal or private communal sewage treatment systems in the vicinity of the subject area.

The local residences including the Whip-Poor-Will Development are serviced by individual on-site sewage disposal (septic) systems. We conclude that the best option for sewage is to service each lot by a single residential treatment system. Therefore, individual on-site sewage disposal systems are proposed for each of the 6 Lots within the subject development.

To determine the impact that 6 new septic systems may have on the environment and groundwater regime, a Hydrogeologic Evaluation Report was prepared by Wilson Associates Ltd. which included a septic system suitability and groundwater impact assessment. The assessment concluded:

Under MECP procedure D-5-4, the nitrate impact of the proposed six lot development is 5.6 mg/L, and well within the maximum acceptable nitrate impact of 10 mg/L. The sewage impact of the proposed six privately-serviced lots will be acceptable.

The findings of the evaluation determined that the subject development can be serviced by Class 4 individual septic systems. Each of the lots is of sufficient size to easily accommodate a private septic system. The Hydrogeological Evaluation is contained in **Appendix C** for reference.

As supported by the Terraprobe Test Pit Geotechnical Investigation, the existing soils have a T time between 4 to 6 min/cm and there was no groundwater in any of the 6 test pits that were completed.

In addition to the above, the appropriate setbacks to both existing and proposed private wells located in the vicinity will be provided in accordance with Ontario Building Code ("OBC").

2.4 Fire Protection

Based on our experience with the Copeland Creek South project, it was agreed in principle that the Township's current tanker truck supply capabilities are adequate to service that proposed development, in addition to other existing developments and residents in the surrounding community. Therefore, the existing wells and the proposed wells on the subject site have not been, and do not need to be, designed to provide fire flows or storage.

3.0 Existing Conditions

3.1 **Topography and Drainage Patterns**

The subject site is currently undeveloped and is comprised almost entirely of wooded cover. All site runoff drains gently northward and ultimately sheet flows towards Copeland Creek, which ultimately discharges into Penetang Bay.

There is a well-defined open ditch along the west side of Overhead Bridge Road. This ditch drains a very small frontage of the subject property but mainly conveys runoff from the Overhead Bridge Road, ROW and asphalt surface. Drainage patterns on the site generally flow from south to north. This site is extremely stable given the existing vegetation.

Refer to the Drainage Plans (Figures 2 and 3) contained in Appendix A.

3.2 Subsurface Conditions

The Soils Map of Simcoe County (Soil Survey Report), published by the Canada Department of Agriculture (1959), reveals that the native soils throughout the subject site area are a Tioga sandy loam, which are classified within hydrologic soils group A.

A test pit investigation has been conducted by Terraprobe Inc. to verify the composition of the native soils. Six test pits which were dug in the probable location of the future septic systems to a depth of approx. 1.4m - 1.8m confirms that the native soils are a sandy material. A standing water elevation was not encountered in any of the test pits upon completion.

Since the vast majority of the subject site are within the Tioga Sandy Loam deposit, and the test pit investigations confirm that the native deposit is a sandy material, all drainage areas will be classified within Hydrologic Soils group 'A' for the purpose of establishing stormwater modelling parameters.

The Subsurface Observations and Geotechnical Comments Report, prepared by Terraprobe, Inc. is contained in **Appendix D** for reference.

4.0 Post-Development Drainage

Post-development drainage patterns will resemble existing drainage patterns as closely as possible. Various low-impact development techniques are also proposed within the drainage system to minimize downstream impacts and disturbance of the wooded landscape.

The Post-Development Drainage Plan (Figure 3) is contained in **Appendix A** for reference. For runoff conveyance design calculations, refer to **Appendix B**.

5.0 Stormwater Management

5.1 Design Criteria Guidelines

The stormwater management design principles for the proposed Overhead Bridge Road 6 Lots Development incorporates the policies and criteria of the Ontario Ministry of the Environment Conservation and Parks (MECP), the Township of Tiny, and utilizes low impact development techniques in various aspects of the stormwater management system.

The stormwater management design criteria for the Overhead Bridge Road 6 Lots Development is as follows:

- The Ontario Government rainfall intensity-duration-frequency (IDF) curves (look up values) are to be used to determine the peak flow rates and runoff volumes generated on the site.
- Major and minor storm flows are to be drained side yard swale and by open ditches on Overhead Bridge Road cross section.
- Quantity controls are not proposed due to the site's close proximity to the discharge point of Copeland Creek into the receiving water body, Penetang Bay. Refer to the Stormwater Management Report, Copeland Creek South Project, Lot 115 Concession 2, Tiny Township, dated January 2016, WMI Project 11-173, for supporting documentation.
- Quality control is required to be provided to MECP 'enhanced' levels (80% total suspended solids removal) through the application of Low Impact Development techniques within the rural road cross section.
- Erosion and sediment control measures will be implemented prior to and during the construction of the development and maintained until the site is stabilized.

5.2 Hydrologic Analysis

5.2.1 Rainfall Data

The hydrologic modelling was completed using the Rational Method to assess the preand post-development peak flows for the site. Storm rainfall distribution was used for the 2, 5, 10, 25, 50, and 100 year storm event calculations.

Refer to **Appendix B** for related calculations.

5.2.2 Pre-Development Condition Results

Using the pre-development drainage area as illustrated in Figure 2 and the program Rational Method, the total flows were determined for the 2, 5, 10, 25, 50, and 100 year storm events. All of the above noted peak flows are summarized in Table 1 below. The hydrologic model runs for the SCS Type-II storm distribution can be found in **Appendix C**. A summary of SWMHYMO input parameters and output results are contained in **Appendix B**.

Catchment	Area (ha)	Rational Method Pre-Development Peak Flows					
		2 yr.	5 yr.	10 yr.	25 yr.	50 yr.	100 yr.
		m³/s m³/s m³/s m³/s m³/s					m³/s
PRE, EX1, EX2	6.16	0.116	0.155	0.180	0.233	0.283	0.325

Table 1: Pre-Development Peak Flows

5.2.3 Post-Development Condition Results

The post-development peak flows for all catchments are summarized in **Table 2** below.

Catchment	Area (ha)	Rational Method Post-Development Peak Flows					
		2 yr.	5 yr.	10 yr.	25 yr.	50 yr.	100 yr.
		m³/s m³/s m³/s m³/s m					m³/s
PRE, EX1, EX2	6.16	0.155	0.206	0.240	0.311	0.377	0.433

Table 2: Post-Development Uncontrolled Peak Flows

In comparing Tables 1 and 2, it is evident that the post-development peak flows slightly exceed the pre-development levels. Quantity controls are <u>not</u> proposed to be provided, however, since the marginal increase in peak flow from this site will have negligible impact on the current capacity of downstream lands. This is due to the watershed's large drainage area of more than 1800ha of land located predominantly upstream of the proposed site area, and the corresponding peak flow 'time to peak' that is much longer than the time to peak from the subject site, therefore rendering the site's increased peak flow impact as minimal.

The post-development drainage recommendations are to control storm runoff on each individual lot. A soakaway pit has been designed for each lot to control flows generated

from the impervious surface of the house as well as the driveway. The sizing of the soakaway pits has been based on a 1:5 year storm event. In our calculations we have not assumed any infiltration from the soakaway pits and this is a very conservative given the highly permeable sandy soils in this area. The house apron area in the driveway will be directed to soakaway pits via perimeter swells. In the event that there is a significant storm event such as the 1:100 year storm it is recommended that interception swales be installed on the upstream side of each individual house apron in order to direct any upstream flows from the upstream lot to the rear of the subject lands. It is our opinion that any runoff during a 1:100 year event will not adversely impact any downstream lands and inclusion of an interception swales is a very conservative measure. This drainage concept is outlined on Figure 4 in **Appendix A** of the report.

5.3 Quality Control

5.3.1 Lot Level Control

To minimize any negative impacts the proposed subdivision may have on the quality of stormwater runoff, an integrated treatment train approach will be implemented.

Specifically, long length grassed swales which will be incorporated into the lot design (by virtue of the large lot sizes) which will promote infiltration of runoff from impervious surfaces into the native sandy soils. These swales will act as enhanced grass swales and serve to function as an LID system.

Additionally, roof downspouts and sump pump discharge from the proposed dwellings will be required to discharge to pervious lawn & landscape areas, so as to further promote infiltration of surface runoff and re-infiltration of groundwater. It should be noted that the proposed landscape features will also provide inherent water balance benefit by way of evapotranspiration and nutrient uptake through vegetation, thus further supporting the hydrologic cycle.

5.4 Source Water Protection

From a source water protection perspective, and based on a review of the South Georgian Bay Lake Simcoe Source Protection Region (Approved South Georgian Bay Lake Simcoe Source Protection Plan, January 26, 2015 - amended February 15, 2018 - and MOECC's Source Protection Atlas), the subject site is located within a Wellhead Protection Area D with a vulnerability score of 2. The application is only for 6 Lots (no commercial), therefore the development and the associated engineering design is not subject to further design requirements related to source water protection (i.e. there are no water quantity threats and as a result a Section 59 Notice is not required).

A copy of an email from Severn Sound Environmental Association is included in **Appendix F**.

5.5 Storm Drainage System & Outlet Design Details

The following summarizes the major features provided within the Stormwater Management system:

- Major and Minor storm flows will be conveyed by swales to Overhead Bridge Road and to the rear of the lots.
- Based on Table 4.4 of the MOE Stormwater Management Planning and Design Manual, March 2003, in order to provide stormwater quality control for a 25mm event over 48 hours the required <u>total storage volume</u> necessary for capture for each house is 5m³. Given we are providing 15m³ per house we have exceeded this requirement.
- Driveway culverts are side based on 1:5 year events with the minimum size being 400mm Ø.

Refer to **Appendix B** for supporting calculations.

6.0 Storm Drainage System Maintenance

The proposed storm soakaway system will require maintenance in order to function properly. The inlets should be inspected at a minimum on a quarterly basis, and after all significant rainfall events (>50mm) to ensure they are not clogged. Recommended operation & maintenance procedures are as follows:

- Sediment and trash deposition on the soakaway pit inlets should be frequently cleaned and disposed of to prevent migration into the roadside ditches, as required. In particular this should be done promptly following major storms and snow melts.
- Grass clippings should not be blown into the ditches to minimize organic loading and prevent clogging.

7.0 Sediment and Erosion Controls

Effective erosion and sediment control must be established prior to construction commencement and maintained until the site has been stabilized. Pro-active measures will be required to limit the amount of sediment travelling down slope. Where site grading is required, exposure of the soil during construction should be minimized to avoid erosion and sedimentation.

<u>Topsoil Stripping:</u> Topsoil stripping will be reduced as much as possible on-site. Where grading is necessary, the exposed soil will be stabilized by seeding immediately upon being set to grade. Should topsoil stockpiling be required, the stockpiles will be kept to manageable levels for grass/weed cutting purposes.

<u>Silt Fence:</u> Silt fence will be placed along the down slope of all excavated material to prevent sediment transport. Periodic inspections and repairs to the silt fence should be performed regularly, as well as after every rainfall event.

<u>Mud Mat:</u> Mud tracking from construction traffic must be controlled through the use of a mud-mat consisting of clear stone located at the site's construction entrance/ exit.

<u>Vegetated Buffers:</u> Existing grassland vegetation/wooded areas along the development limits are to be maintained wherever possible. These areas will provide a natural barrier to filter potentially sediment-laden overland flow before it is released from the site.

Finally, the site Engineer Building Contractor will be responsible for completing routine inspections of the sediment and erosion control structures throughout the construction phase of the development, particularly after rainfall events. All damaged or clogged control devices or fencing must be repaired immediately.

8.0 Traffic Impact Brief

8.1 Background

The subject site is located at the northwest corner of Overhead Bridge Road and Concession Road 12 East and is to comprise 6 residential Lots.

It is bound by existing single family residential developments to the north, south and west, which front onto Overhead Bridge Road and local residential roads such as Whippoor-will Drive and Kingfisher Crescent and Goldfinch Crescent. 5 of the 6 proposed lots are to have their driveway accesses directly onto Overhead Bridge Road. One Lot will have access to Concession 12.

8.2 Traffic Volume Impacts

Trip generation rates were determined using the Institute of Transportation Engineers' (ITE) Trip Generation Manual, 10th Edition. The single family detached housing dataset (code # 210) provides a wide range of statistical data from a number of sites that are similar in nature to the proposed development; as such this data was utilized for the subject site. The data for the 'Weekday Peak hour of Adjacent Street Traffic, One Hour Between 7am and 9am' time period is utilized throughout this analysis since it results in conservative estimates of trips and is representative of peak travel periods in residential neighborhoods such as this.

Using the fitted curve equation from the 'Weekday Peak hour of Adjacent Street Traffic, One Hour Between 7am and 9am' report, ten (10) total vehicular trips (entering and exiting) are expected to be generated by this development. Refer to the Trip Generation Spreadsheet appended to this Brief for calculation details. From the review of the local road networkand likely travel destinations such as shopping centers, employment lands, recreation facilities/attractions relative to the location of the primary arterial roads through the Township (namely County Roads 6, 25, 26, and 93), it is estimated that the majority of vehicular trips generated from the development will travel to/from the south via Overhead Bridge Road, Concession Road 11 East and Golf Link Road.

The minor increase in vehicular trips as a result of the proposed development is insignificant and will have little to no effect on traffic movements and capacities on existing roadways and the stop controlled intersections in the local area. Therefore, it is expected that the development can be accommodated within the existing transportation system without retrofits or improvements.

8.3 Sight-Distance Analysis

Ontario's Ministry of Transportation (MTO) outlines specific sight-distance geometry criteria to ensure safe vehicular movement to and from intersecting roadways and to ensure that through traffic on the adjacent roadway will have adequate time and space for manoeuvrability and braking. Based on a design speed of 80km/hr (10 km/hr over the posted speed of 70km/hr), the minimum required stopping sight-distance is approximately 130m (referenced from MTO Geometric Design Standards for Ontario Highways Manual, Figure E3-6). The minimum safe sight distance for vehicles turning left or right onto a two-lane highway and assuming the operating speeds before being overtaken by vehicles travelling in the same direction (condition D and E east, as referenced from figure E3-6) is approximately 270m. Refer to the appended E3-6 figure for sight-distance calculation details.

From review of existing site conditions and sight-lines from the vantage point of the proposed Lots 1 to 5 driveway access at Overhead Bridge Road, visibility is noted to be adequate to achieve the minimum stopping sight distance, since there are no notable obstructions and the road alignment is relatively straight from this location up to and including 130m away in either direction. There is a slight curve in Overhead Bridge Road to the south of the subject site, which does slightly restrict the available sight-distance to an estimated 240m from the vantage point of Lot #6 at Overhead Bridge Road but as the driveway access for Lot 6 is from Concession 12, this is not an issue. However, the remaining frontage of the property does have sight-distance visibilities in excess of 270m.

8.4 Traffic Impact Summary

This design brief demonstrates that the proposed Charlebois development between 584 and 564 Overhead Bridge Road can be accommodated within the local community without adverse impacts on existing transportation systems. In particular, the estimated 10 peak hourly trips onto Overhead Bridge Road is relatively insignificant in terms of traffic volume, and should be easily accommodated by existing roads. Also, the sight-distance onto Overhead Bridge Road is noted to be generally adequate based on MTO design guidelines with the current posted speed of 70km/hr.

9.0 Summary and Conclusions

This Functional Servicing and Stormwater Management Report demonstrates how the proposed Overhead Bridge Road 6 Lots can be serviced and integrated into the existing community, without imposing any adverse effects. Specifically, we note the following:

- The 6 Lots can be adequately supplied with potable drinking water via the installation of individual drilled wells located on each lot.
- Sewage disposal can be achieved by installing a conventional Class 4 disposal system on each lot.
- Stormwater quality control will be achieved in the conveyance system to MECP enhanced levels by retaining runoff in soakaway pits, for infiltration into the native sandy soil. These lot level controls will be provided to further promote infiltration of impervious surface runoff.
- The use of silt fence, mud mats, and existing vegetated buffers will ensure downstream stormwater quality is maintained during construction.

We confirm the development of the 6 Lots can be achieved and recommendations of this report can support the Planning Application.

Respectfully submitted,

WMI & Associates Limited

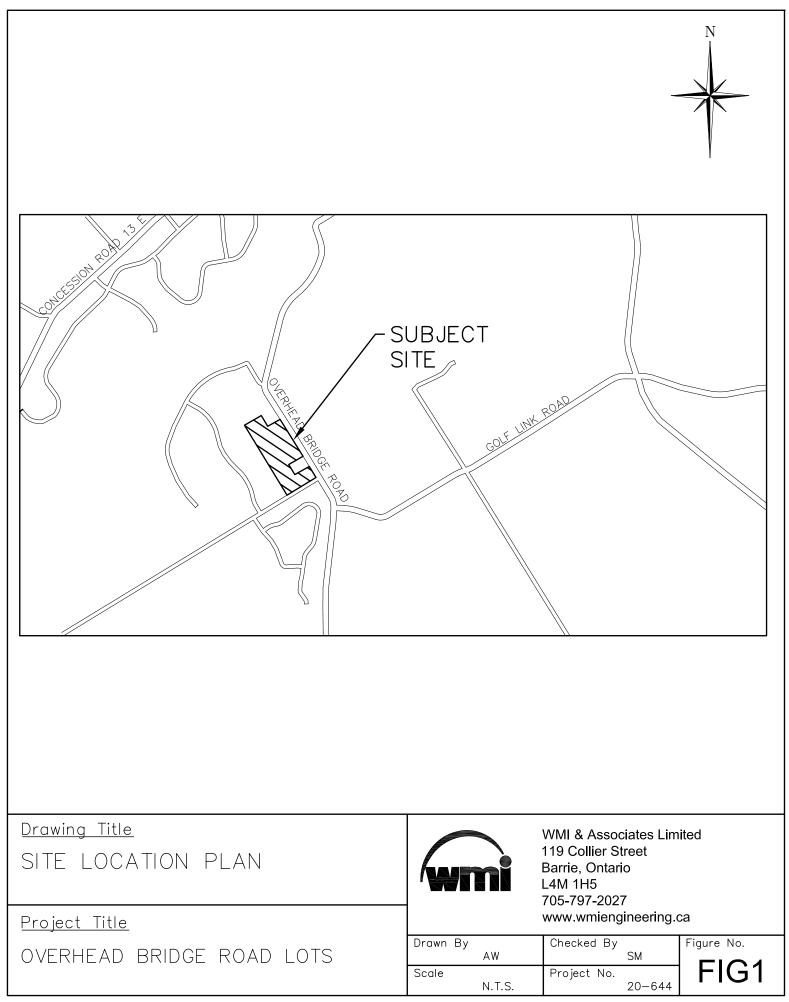
A. moras

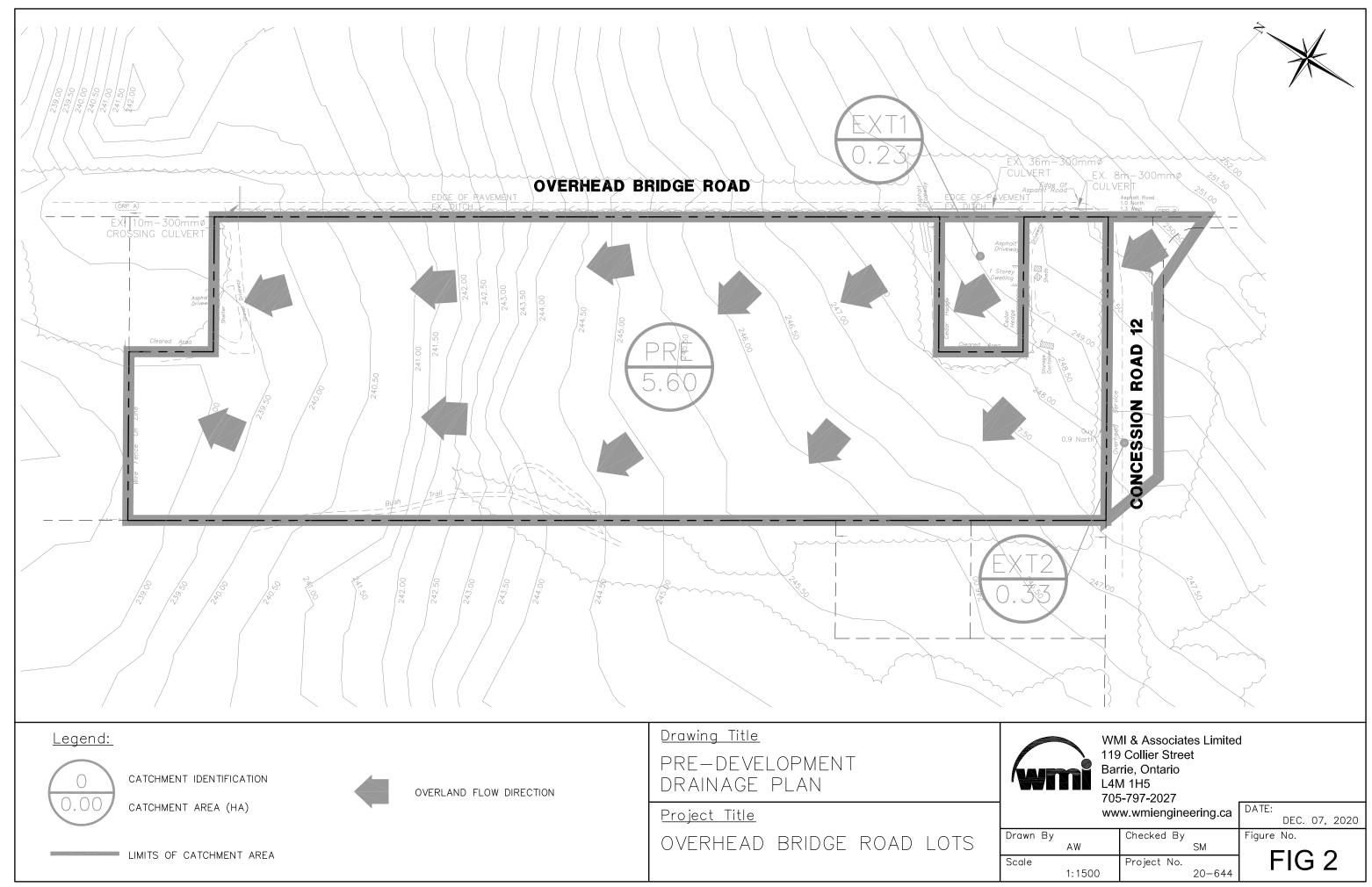
Stephen Morash, P.Eng.

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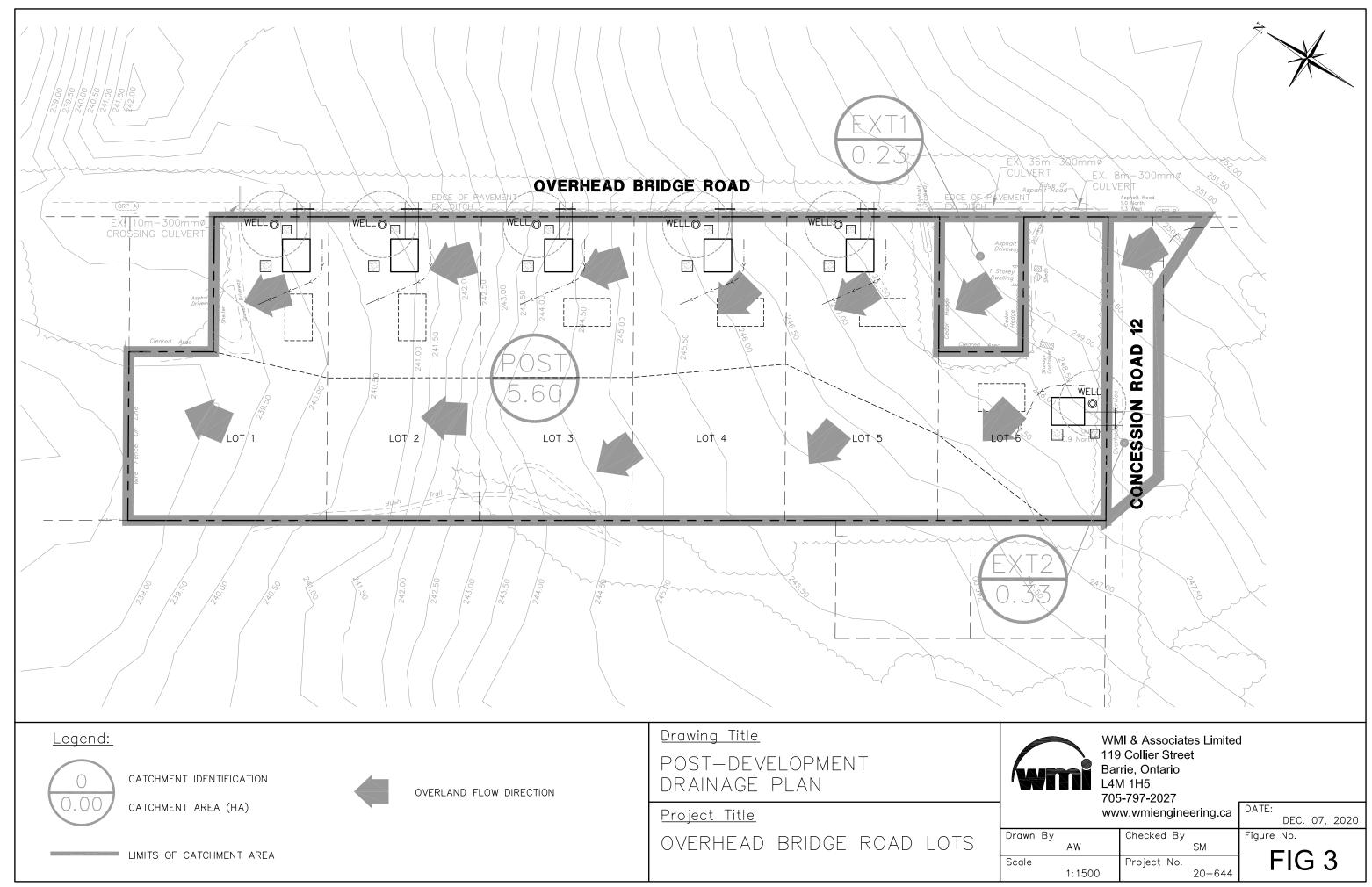
Figures & Drawings

APPENDIX A





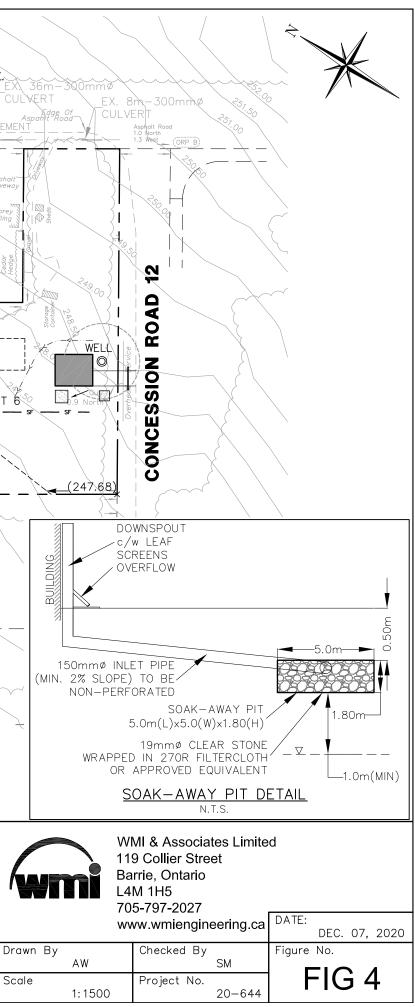
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\\WMI-SERVER\wmi-server\Data\Projects\2020\20-644\CAD\WMI\Issue_No1\201126_20-644_Base.dwg,FIG3,1:1

(REFER TO DETAIL ON THIS SHEET)	TEAD BRIDGE ROAD
EX 10m-300mm Ø CROSSING CULVERT	WELLO WELLO Striveway
SEPTIC 250m ² SEPTIC 250m ² (TYP,)) Autor Existing Autor	ED PÉR 199
Legend: PR. 2000ft ² BUILDING (240.55) PR. MATCH EXISTING PR. 2000ft ² BUILDING (240.55) PR. MATCH EXISTING ELEVATIONS PR. SEPTIC SYSTEM PR. SOAK-AWAY PIT PR. SOAK-AWAY PIT PR. DRILLED WELL	EMENT Drawing Title SITE SERVICING & GRADING PLAN Project Title OVERHEAD BRIDGE ROAD LOTS

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APPENDIX B

Stormwater Management Calculations



WMI & Associates Limited 119 Collier Street, Barrie, Ontario L4M 1H5 p (705) 797-2027 f (705) 797-2028

RUNOFF COEFFICIENT CALCULATIONS "C" SPREADSHEET

Date: 2020-12-07

Project No.: 20-644

Project: Overhead Bridge Road

Prepared By: BD

RUNOFF COEFFICIENT NUMBERS

	Land Cover	Hydro	Hydrologic Soil Groups				
		A-AB	B-BC	C-D			
	0 - 5% grade	0.22	0.35	0.55			
Cultivated Land	5 - 10% grade	0.3	0.45	0.6			
	10 - 30% grade	0.4	0.65	0.7			
	0 - 5% grade	0.1	0.28	0.4			
Pasture Land	5 - 10% grade	0.15	0.35	0.45			
	10 - 30% grade	0.22	0.4	0.55			
Woodlot or Cutover	0 - 5% grade	0.08	0.25	0.35			
	5 - 10% grade	0.12	0.3	0.42			
	10 - 30% grade	0.18	0.35	0.52			
Lakes and Wetlands		0.05	0.05	0.05			
Impervious Area	(i.e. buildings, roads, parking lot, etc.)	0.95	0.95	0.95			
Gravel	(not used for proposed parking or storage areas)	0.4	0.5	0.6			
Desidential	Single Family	0.3	0.4	0.5			
Residential	Multiple (i.e. semi, townhouse, apartment, etc.)	0.5	0.6	0.7			
Industrial	Light	0.55	0.65	0.75			
industrial	Heavy	0.65	0.75	0.85			
Commercial		0.6	0.7	0.8			
Unimproved Areas		0.1	0.2	0.3			
•	< 2% grade	0.05	0.11	0.17			
Lawn	2 - 7% grade	0.1	0.16	0.22			
	> 7% grade	0.15	0.25	0.35			

Ref: Runoff Coefficient Numbers - Adapted from Design Chart 1.07, Ontario Ministry of Transportation, "MTO Drainage Management Manual", MTO. (1997)

<<< Elements Requiring Input Information</p>

PRE-DEVELOPMENT CONDITION

	Land Cover	Hydro	logic Soil G	iroups
		A-AB	B-BC	C-D
	0 - 5% grade			
Woodlot or Cutover akes and Wetlands mpervious Area Gravel Residential ndustrial Commercial	5 - 10% grade			
	10 - 30% grade			
	0 - 5% grade			
Pasture Land	5 - 10% grade			
asture Land Voodlot or Cutover akes and Wetlands npervious Area iravel tesidential ndustrial commercial Inimproved Areas	10 - 30% grade			
	0 - 5% grade	5.73		
Woodlot or Cutover	5 - 10% grade			
	10 - 30% grade			
Lakes and Wetlands				
Impervious Area	0 - 5% grade sture Land 5 - 10% grade 10 - 30% grade 0 - 5% grade 0 - 30% grade 0 - 30% grade 0 - 30% grade 0 - 30% grade (i.e. buildings, roads, parking lot, etc.) avel (not used for proposed parking or storage areas) sidential Single Family Multiple (i.e. semi, townhouse, apartment, etc.) Light Heavy	0.30		
Gravel	(not used for proposed parking or storage areas)			
Residential	Single Family			
Pasture Land Woodlot or Cutover Lakes and Wetlands Impervious Area Gravel Residential Industrial Commercial Unimproved Areas	Multiple (i.e. semi, townhouse, apartment, etc.)			
Industrial	Light			
industrial	Heavy			
Commercial				
Unimproved Areas				
	< 2% grade	0.13		
Residential Industrial Commercial	2 - 7% grade			
	> 7% grade			

Total Area (ha) = 6.16

POST-DEVELOPMENT CONDITION

	Land Cover	Hydro	logic Soil G	iroups
		A-AB	B-BC	C-D
	0 - 5% grade			
Cultivated Land Pasture Land Voodlot or Cutover akes and Wetlands mpervious Area Gravel Residential Commercial Jnimproved Areas	5 - 10% grade			
	10 - 30% grade			
	0 - 5% grade			
Pasture Land	5 - 10% grade			
Pasture Land Voodlot or Cutover akes and Wetlands mpervious Area Bravel Residential Industrial Commercial Jnimproved Areas	10 - 30% grade			
asture Land Voodlot or Cutover akes and Wetlands npervious Area iravel tesidential ndustrial commercial Inimproved Areas	0 - 5% grade	5.13		
Woodlot or Cutover	5 - 10% grade			
	10 - 30% grade			
Lakes and Wetlands				
Impervious Area	(i.e. buildings, roads, parking lot, etc.)	0.60		
Gravel	(not used for proposed parking or storage areas)			
Desidential	Single Family			
Residential	Multiple (i.e. semi, townhouse, apartment, etc.)			
امطربمتها	Light			
industrial	Heavy			
Commercial				
Unimproved Areas				
	< 2% grade	0.43		
Lawn	2 - 7% grade			
	> 7% grade			

Total Area (ha) = 6.16

Runoff Coefficient, C = 0.16

\\WMI-SERVER\wmi-server\Data\Projects\2020\20-644\Design\Storm\[2_201207_Rational_Method_Calcs(A,B).xlsx]Rational Method

WMI & Associates Limited 119 Collier Street, Barrie, Ontario L4M 1H5 p (705) 797-2027 f (705) 797-2028



I.D.

PRE

POST

(ha)

6.16

6.16

(min.)

15.0

15.0

RATIONAL METHOD CALCULATIONS

Date: 2020-12-07

Project No.: 20-644

Project: Overhead Bridge Road

Prepared By: BD

<<< Element

Elements Requiring Input Information

Rainfall Intensity-Duration-Frequency Coefficients from: http://www.mto.gov.on.ca/IDF_Curves/terms.shtml

2-year		5-у	vear	10-	10-year		/ear	50-	year	100	-year
A =	21.5	A =	28.6	A =	33.3	A =	39.2	A =	43.6	A =	48.0
B =	-0.699	B =	-0.699	B =	-0.699	B =	-0.699	B =	-0.699	B =	-0.699
		Ratio	nal Method Fo	ormula		Rainfa	III Intensity I	Equation (2-100	0 year storm	events)	
	Q	=		<u>I x A</u> 60	(m ³ /s)	I ₂₋₁₀₀	=	A x (T	_C / 60) ^B	(mm/hr)	
	where,	C = =	Runoff Coeff Rainfall Inter	icient sity, (mm/hr)		where,	A = B =	Rainfall IDF Rainfall IDF			
		A =	Drainage Are	ea, (ha)			$T_{C} =$	Time of Con	centration, (n	nin)	
	Runoff Coefficient Equations Based on MTO Drainage Manual (1984), page BD-4						ty Equation (25 DE SWMP Man				
	2-year	•		//1-5-		I _{25mm}	=		C) + 5.9	(mm/hr)	
	5-year	C ₅ =	С								
	10-year	C ₁₀ =	С			where,	C =	Runoff Coeff	ficient		
	25-year	C ₂₅ =	1.10 x C								
	50-year	C ₅₀ =	1.20 x C								
	100-year	C ₁₀₀ =	1.25 x C								
	For storms ha	aving a returr	n period of mo	ore than 10 ye	ars, the						
	Runoff Coefficient, C, will be increased as indicated above, up to										
	a maximum value of 1.										
Catchment	Α	Tc	С	Q _{25mm}	Q ₂	Q ₅	Q ₁₀	Q ₂₅	Q ₅₀	Q ₁₀₀	1

(m³/s)

0.116

0.155

(m³/s)

0.155

0.206

(m³/s)

0.180

0.240

(m³/s)

0.233

0.311

(m³/s)

0.283

0.377

(m³/s)

0.325

0.433

\\WMI-SERVER\wmi-server\Data\Projects\2020\20-644\Design\Storm\[2_201207_Rational_Method_Calcs(A,B).xlsx]Rational Method

0.12

0.16

(m³/s)

0.023

0.035



WMI & Associates Limited 119 Collier Street, Barrie, Ontario L4M 1H5 p (705) 797-2027 f (705) 797-2028

STORMWATER MANAGEMENT CALCULATIONS SOAKAWAY PIT DESIGN

Date: 2020-12-02

Project No.: 20-644

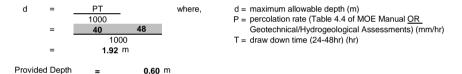
Project: Overhead Bridge Road

Prepared By: BD

Purpose: An soakaway pit is proposed on each lot to provide quality control, water balance, volume control and phosphorus reduction benefits. The soakaway pits will be sized to store the entire runoff volume generated by the contributing building rooftop area during a 25mm storm event while maintaining a maximum draw down time of 48 hours. **Elements Requiring Input Information** <<< Infiltration Volume: Total Area 0.02 ha Runoff Volume 25 mm Infiltration Volume A (ha) x RV (mm) x 10 m 0.02 ha 25 mm x 10 х m³ = 5 m³ =

Max. Allowable Depth:

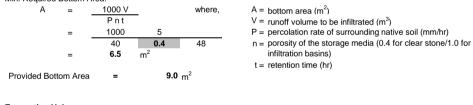
Based on the Ministry of the Environment's (MOE) Stormwater Management Design Manual dated March 2003, Page 4-20, Equation 4.2: Maximum Allowable Depth is:



Min. Bottom Area:

Based on the Ministry of the Environment's (MOE) Stormwater Management Design Manual dated March 2003, Page 4-26, Equation 4.3: Infiltration Bottom Area is:

Min. Required Bottom Area:



Excavation Volume:

Min. Required Excavation Volume	=	Infiltration Volume/por	osity of the storage media
	=	5	
		0.4 <	(0.4 for clear stone/1.0 for infiltration basins)
	=	12.5 m ³	
Provided Excavation Volume	=	LxWxD m ³	
	=	3 m x	3 m x 0.6 m
	=	5.4 m ³	

Soil Cover: Based on the Ministry of the Environment's (MOE) Stormwater Management Design Manual dated March 2003, Page 4-21, Figure 4.4: Soil Cover for Trenches (based on frost heave potential).



Notes: - Refer to the latest Geotechnical Letter for the percolation rate which was estimated to be 4-6min/cm (100mm/hr) through grain size distribution analyses. Considering this, and based on Table C1 in Appendix C of the LID Design Guide and assuming that the soil horizon is continuous within 1.5m below the proposed bottom of the infiltration features, the mean infiltration rate assumed (100mm/hr) has been divided by a safety correction factor of 2.5 to calculate the design infiltration rate of 40mm/hr. Refer to Table C2 in Appendix C of the LID Design Guide for reference to the safety correction factor noted above. Groundwater was not encountered on-site.

\\WMI-SERVER\wmi-server\Data\Projects\2020\20-644\Design\Storm\{4_201202_Infiltration_Feature_Design(MOE).xlsx]Infiltration Pit

Culvert Calculator Report 20-644 Driveway Culvert

Comments: Driveway Culvert sized to convey peak flows generated by the 5-year design storm (1.50ha contributing area - 0.082cu.m/s).

Minimum culvert size of 400mm (CMP) required at a minimum slope of 0.5%

Solve For: Headwater Elevation

Culvert Summary					
Allowable HW Elevation	0.44	m	Headwater Depth/Height	0.87	
Computed Headwater Eleva	0.40	m	Discharge	0.0820	m³/s
Inlet Control HW Elev.	0.36	m	Tailwater Elevation	0.00	m
Outlet Control HW Elev.	0.40	m	Control Type	Outlet Control	
Grades					
Upstream Invert	0.04	m	Downstream Invert	0.00	m
Length	9.00	m	Constructed Slope	0.005000	m/m
Hydraulic Profile					
Profile	M2		Depth, Downstream	0.20	m
Slope Type	Mild		Normal Depth	0.33	m
Flow Regime	Subcritical		Critical Depth	0.20	m
Velocity Downstream	1.26	m/s	Critical Slope	0.019060	m/m
Section					
Section Shape	Circular		Mannings Coefficient	0.024	
Section Material	CMP		Span	0.41	m
Section Size	400 mm		Rise	0.41	m
Number Sections	1				
Outlet Control Properties					
Outlet Control HW Elev.	0.40	m	Upstream Velocity Head	0.04	m
Ke	0.90		Entrance Loss	0.03	m
Inlet Control Properties					
Inlet Control HW Elev.	0.36	m	Flow Control	Unsubmerged	
Inlet Type	Projecting		Area Full	0.1	m²
К	0.03400		HDS 5 Chart	2	
М	1.50000		HDS 5 Scale	3	
С	0.05530		Equation Form	1	
Υ	0.54000				

APPENDIX C

Hydrogeological Assessment (by Wilson Associates Inc.)

Ian D. Wilson Associates Ltd. *since 1974*

December 5, 2020

Mr. Frank Charlebois Charlebois Properties Inc. 430 Concession 16 East Tiny, ON L9M 0P1

Dear Mr. Charlebois:

Re: Desktop Hydrogeological Assessment - Proposed Residential Lots Overhead Bridge Road at Concession Road 12 Part Lot 9, Concession 12, Township of Tiny

It is proposed to develop six residential lots on a 5.5968ha parcel of land located at the northwest corner of the intersection of Overhead Bridge Road and Concession Road 12, within part of Lot 9, Concession 12, Township of Tiny. The attached drawing, prepared by Celeste Philips Planning Inc., shows the location and layout of the proposed lots.

It is proposed to service the lots with individual drilled water wells and private subsurface sewage disposal systems.

To support the development proposal, a desktop hydrogeological study was conducted involving the following:

- A desktop review of readily available background hydrogeological information for the site and vicinity.
- A review of site-specific subsurface information detailed in the December 3, 2020 Test Pit Investigation letter report from Terraprobe Inc. (copy attached).
- Sewage system development impact assessment under current Ministry of the Environment, Conservation and Parks (MECP) Procedure D-5-4 "Technical Guideline For Individual On-Site Sewage Systems : Water Quality Impact Risk Assessment", commonly known as the "nitrate guideline".
- A review of water well records to provide comment regarding aquifer conditions and groundwater supply potential.

This desktop study was completed at the request of Charlebois Properties Inc.

Tel: 519.233.3500 Fax: 519.233.3501 P. O. Box 299 Clinton, Ontario NOM 1L0

Wilson Associates

Consulting Hydrogeologists

Hydrogeology

SITE SETTING, GEOLOGY AND HYDROGEOLOGY

The proposed development is located northwest corner of the intersection of Overhead Bridge Road and Concession Road 12. The site is a mostly rectangular parcel, with two existing residential lots dividing the frontage on Overhead Bridge Road. Total frontage on Overhead Bridge Road is about 365m and frontage along Concession Road 12 is about 137m. The subject lands are forested and undeveloped. The site exhibits a slope to the north or northwest, with a total relief of about 10m. Lands to the west, north and south are occupied by residential lots. Apart from the two existing residential lots fronting on Overhead Bridge Road, lands to the east are undeveloped forest.

No surface water bodies are located on or in the close vicinity of the site. Simcoe County website mapping suggests that wetland conditions may be present downslope to the north of the site.

The subject property is situated within the Simcoe Uplands physiographic region of southern Ontario, which consists of a series of rolling till plains situated above the glacial Lake Algonquin shoreline. According to Ontario Geological Survey Map P.975 "Quaternary Geology of the Orr Lake - Nottawasaga Area", the upper soils consist of glaciolacustrine shallow water deposits of sand with minor fine gravel. The Terraprobe report indicates that all subsurface samples collected consisted of sand with traces of gravel and/or silt, consistent with Quaternary geology mapping.

According to the record of a log of a 1978 test well completed about 1.5km to the southwest, (Well Record # 5715544), the overburden is approximately 100 to 110 metres deep in the vicinity of the site. Nearby well records report that the upper half of the overburden largely consists of granular deposits of sand, or sand and gravel, with discontinuous, variable fine-grained deposits at depths typically in the range of 20m to 40m below grade. Distant well records typically report the lower overburden to be fine-grained in character.

The bedrock beneath the site consists of limestone or dolostone of the Simcoe Group.

The majority of local groundwater supplies are obtained from the granular deposits of the intermediate overburden. The lower overburden typically provides little to no potential for groundwater supply due to its fine-grained character, and the bedrock is less often utilized due to the expense of deep drilling and the potential of obtaining aesthetically poor-quality water.

WELL POTENTIAL ANALYSIS

To establish well yield and basic water quality probabilities, up-to-date MECP records for water wells located within approximately 500 metres of the proposed development were reviewed. Records for well abandonments, geotechnical or environmental monitoring wells are not included in the summary. The MECP water well record database contains the records for 18 water wells within the review area. The water well records used in the preparation of the review are attached. The following summarizes the reported well record information within the review area.

Number of wells:	18
Drilled Construction:	18
Dug/Bored Construction:	0
Sandpoint Construction:	0
Unknown Construction:	0
Completed in Overburden:	18 (100%)
Completed in Bedrock:	0

The following summarizes the reported well performance data.

1	Maximum	Minimum	Average
Well Depth (m)	74.7	29.6	57.2
Test Rate (L/min)	455	23	78
Test Period (Hours)	24	1	4.5

Reported Water Quality:

Fresh:	18 or 100% (no objectionable tastes or odours)
Sulphurous:	none
Mineralized/Saline:	none
Quality Not Reported:	none
Dry Well:	none

The average reported well within about 500 metres of the proposed development is of drilled construction, completed in the intermediate overburden to a depth of 57.2metres and yields 78 litres of fresh-quality water per minute over an average period of 4.5 hours. This average yield significantly exceeds the maximum water demand of a normal four bedroom home specified by the MECP (i.e. 18L/min without inline storage). Overall groundwater conditions are very favourable for domestic water requirements. The high average well yield in the vicinity of the site is consistent with an aquifer setting that is more than capable of supplying domestic water demand with limited risk of adverse interference on the large lots proposed.

It should be noted that the above summary and analysis is based solely on information contained in the MECP water well record database as reported by drilling contractors and is not

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subject to quality control, however the overall analytical summary is very favourable.

WATER QUALITY

Based on the probable depth of on-site wells (i.e. ±57m) in the intermediate overburden, the bacteriological quality of water from properly-constructed wells is anticipated to be acceptable. Samples of water collected in 1992 by Wilson Associates from Whippoorwill Well #2 (Well Record No. 5728953), completed about 300m to the south and in the same overburden aquifer in which the on-site wells are likely to be completed, were reported to contain no detectable Total Coliform or E. Coli bacteria (analysis attached). The Tiny Township 2019 Annual Drinking Water Report for the Whippoorwill Wells 1 and 2 reports that 104 samples of raw water were collected from the Whippoorwill wells, with non-detectable to low (1 CFU/100mL) Total Coliform and no detectable E. Coli bacteria (attached).

The chemical quality of groundwater from the intermediate overburden aquifer is known to be acceptable. Samples of water collected by Wilson Associates in 1992 from Whippoorwill Well #2 (Well Record No. 5728953), completed about 300m to the south and in the same overburden aquifer in which the on-site wells are likely to be completed, were reported to be slightly alkaline (pH 7.92) and to exhibit moderate hardness (198mg/L as CaCO₃) (analyses attached). All parameters determined in 1992 were at acceptable levels, with no indicators of surface water impact (i.e. elevated levels of nitrate, chloride, sodium, etc...). The Tiny Township 2019 Annual Drinking Water Report for the Whippoorwill system reports no applicable chemical water quality exceedances of the Ontario Drinking Water Quality Standards (attached).

SEWAGE SYSTEM IMPACT ASSESSMENT

Under the current MECP "Technical Guideline For Individual On-Site Sewage Systems : Water Quality Impact Risk Assessment" (Procedure D-5-4, also known as the "nitrate guideline"), each proposed development of five lots or greater utilizing individual on-site sewage systems requires an assessment of groundwater impact potential. The purpose of the assessment is to ensure that the discharge from the individual on-site sewage systems will have a minimal effect on groundwater and the present or potential use of adjacent properties. The assessment involves a three-step process, with the need to advance to the next step dependant on the requirements of the previous step. Where the background nitrate content of shallow groundwater exceeds 10 mg/L, additional development cannot normally be supported.

Based on samples collected from the nearby Whippoorwill wells (per the 2019 Annual Drinking Water Report), the nitrate content of groundwater is low, recently ranging between 0.2 and 0.7mg/L.

Under Step 1 of the guideline, for developments where the lot size for each private residence within the development is one hectare or larger (with no lots being less than 0.8ha in area), the risk that the limits imposed by the guideline may be exceeded is considered acceptable with no additional hydrogeologic assessment. Step 1 of the guideline is not applicable based on lot size.

Ian D. Wilson Associates Limited

Step 2 of the guideline is applicable where groundwater resources can be confidently demonstrated to be hydraulically isolated from potential sewage pathways. As the upper overburden is predominantly granular, Step 2 of the guideline does not apply.

Under Step 3 of the guideline, a mass-balance calculation is used to determine the potential impact of the proposed lots. Under the current MECP guideline only infiltrating precipitation and the volume of water contained in the sewage may be considered as dilutants for the nitrate contained in septic effluent. To establish the infiltration rate, the percentage of the local water surplus which may infiltrate is calculated using the Rational Method approach. According to the Terraprobe soil evaluation and Quaternary geology mapping, the upper soil profile consists of sand (infiltration factor 40%), the overall relief is hilly (infiltration factor 10%) and the cover will likely be cleared (infiltration factor 10%), all resulting in an infiltration factor of 60%. The water surplus for the site is assumed to be 456mm/year, based on the 1981-2010 precipitation normal for the closest Environment Canada weather station - Midland WPCP weather station (1040.6mm/year, rounded to 1041mm/year) and the actual evapotranspiration rate as identified for Copeland Creek subwatershed by the 2015 Severn Sound Source Protection Area Approved Assessment Report (Table 3.2-3 - actual evapotranspiration 585mm/year).

As such, the annual infiltration rate will be 273mm (60% of 456mm), representing about 26% of average annual precipitation in the sub-watershed.

The following mass-balance formula is used to calculate the impact of the proposed development under the MECP guideline:

$$Q_{T}C_{T} = Q_{S}C_{S} + Q_{P}C_{P}$$

Where:

 Q_T = Sum of Q_S and Q_P C_T = Nitrate concentration

 $C_{\rm T} = Nillale concentration$

Q_s = Volume of sewage (6 lots @ 1000 L/day/lot, per MECP guideline)

 $C_s = Nitrate content of sewage (40 mg/L, per MECP guideline)$

 Q_{p} = Infiltration (273mm/year x 5.5968ha x 10,000L/mm/ha = 1.53x10⁷L/yr)

 C_{p} = Nitrate content of shallow groundwater (0.7mg/L assumed, see above)

Therefore:

 $(2.19 \times 10^{6} \text{L/yr} + 1.53 \times 10^{7} \text{L/yr}) \times C_{\tau} = (2.19 \times 10^{6} \text{L/yr} \times 40 \text{mg/L}) + (1.53 \times 10^{7} \text{L/yr} \times 0.7 \text{mg/L})$ C_T = 5.6 mg/L

Based on the MECP-specified daily volume of sewage for the purposes of the Procedure D-5-4 assessment, and an infiltration rate of 273mm/year, the nitrate impact of the proposed six-lot development is 5.6mg/L, and well within the maximum acceptable nitrate impact of 10mg/L. As such, the sewage impact of the proposed six privately-serviced lots will be acceptable.

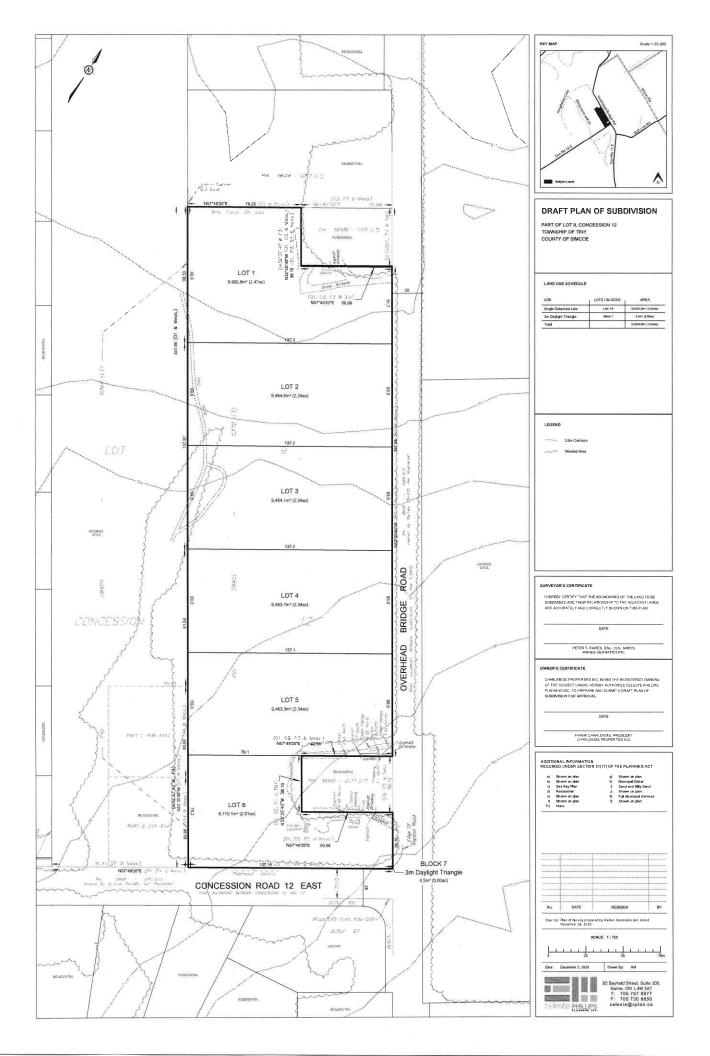
CONCLUSIONS AND RECOMMENDATIONS

- 1. The average reported well within about 500 metres of the proposed development is of drilled construction, completed in the intermediate overburden to a depth of 57.2metres and yields 78 litres of fresh-quality water per minute over an average period of 4.5 hours. This average yield significantly exceeds the maximum water demand of a normal four bedroom home specified by the MECP (i.e. 18L/min without inline storage). Overall groundwater conditions are very favourable for domestic water requirements. The high average well yield in the vicinity of the site is consistent with an aquifer setting that is more than capable of supplying domestic water demand with limited risk of adverse interference on the large lots proposed.
- 2. Based on historical and on-going water quality analytical data from the nearby Whippoorwill wells, which are completed in the same overburden aquifer in which the on-site wells are likely to be completed, the bacteriological and chemical quality of water from properly-constructed on-site drilled wells will be acceptable.
- 3. Under MECP Procedure D-5-4, the nitrate impact of the proposed six-lot development is 5.6mg/L, and well within the maximum acceptable nitrate impact of 10mg/L. The sewage impact of the proposed six privately-serviced lots will be acceptable

Should there be any questions regarding the above information and discussion, please do not hesitate to contact this office.

IAN D. WILSON ASSOCIATES LIMITED

Geoffrey Rether, B.Sc., P.Q **GEOFFREY B. RETHER** PRACTISING MEMBER 0426 VTAR



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Branch Laboratoire de Date Rec Branch Laboratoire Date Rec Bacteriological (Mais b) (Asis b) (Mais r 3) Analyse Bactériologique de l'eau	$\mathcal{L}\mathcal{P}, \mathcal{C}\mathcal{I}\mathcal{I}, \mathcal{T}\mathcal{N}$	IAND. WLSON 4560C Street, R.R., Box No. / Rue, R.R., Caster Pustal ROX 7 7 7	(Trop)	is box. Drinking water only e case. Eau potable seulen turther information. / Pour les directives	CHECK APPROPRIATE BOXES / COCHER TOUTES LES CAPES APPROPRIFES	NON-DRINKING WATER	Hydrotherapy Swimming Spa, Whitpool Pool-Outdoor Wading Pool Swage	Other	ICTERIES BACTERIAL Interest COUNT Mume de 100 ml Based on 10 ml	-	a saureus PUBL	
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ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO, K2E 7T7 TELEPHONE: (613) 228 1145 FAX: (613) 228 1148

ABORATORY I.D.: 140192-2 AMPLE MATRIX: Well Water, Bidan Subdivision EPORT NUMBER: 7943001			CLIENTS JOB NUMBER: DATE SUBMITTED: DATE REPORTED:	Ian D. Wilson, 89-19 14-01-92 30-01-92		
DRINKING WATER CRITERIA	UNITS		RESULTS			
PARAMETERS		Well 2 Tiny Twp.				
Colour	T.C.U.	<1				
Hardness(CaCO $_3$)	mg/L	198				
Alkalinity(CaCO₃)	mg/L	149				
Turbidity	N.T.U.	11				
Conductivity	uS/cm	390				
pH		7.92				
Fluoride	mg/L	<0.1				
Chloride	mg/L	3.7				
Nitrite (N)	mg/L	<0.1				
Nitrate (N)	mg/L	< 0.1				
Sulphate	mg/L	20.3				
Calcium	mg/L	51.8				
Magnesium	mg/L	16.6				
Sodium	mg/L	6.4				
Potassium	mg/L	2.6				
Ammonia (N)	mg/L	0.16				
TKN	mg/L	0.2				
Cyanide	mg/L	< 0.02				
Phenols	mg/L	< 0.002				
тос	mg/L	1				
DOC	mg/L	1				

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ABORATORY I.D.: 140192-2 AMPLE MATRIX: Well Water, Bidan Subdivision EPORT NUMBER: 7943001		bdivision	CLIENTS JOB NUMBER: DATE SUBMITTED: DATE REPORTED:	Ian D. Wilson, 89-19 14-01-92 30-01-92		
DRINKING WATER CRITERIA	UNITS		RESULTS			
PARAMETERS		Well 2 Tiny Twp.				
Barium	mg/L	0.11				
Cadmium	mg/L	< 0.004				
Chromium	mg/L	< 0.01				
Copper	mg/L	< 0.01				
Arsenic	mg/L	< 0.01				
Boron	mg/L	· 0.01				
Iron	mg/L	0.02				
Lead	mg/L	< 0.04				
Manganese	mg/L	0.034				
Selenium	mg/L	< 0.005				
Silver	mg/L	< 0.01				
Zinc	mg/L	0.03				
Mercury	mg/L	< 0.001	а. — — — — — — — — — — — — — — — — — — —			
Uranium	mg/L					

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SAMPLE MATRIX: Well	PLE MATRIX: Well Water, Bidan Subdivision		CLIENTS JOB NUMBER: DATE SUBMITTED: DATE REPORTED:	Ian D. Wilson, 89-19 14-01-92 30-01-92		
DRINKING WATER CRITERIA	UNITS		RESULTS			
PARAMETERS		Well 2 Tiny Twp.				
Anion Sum	meq/L	3.98				
Cation Sum	meq/L	4.30				
% Difference	%	3.81				
Ion Ratio	AS/CS	0.93				
Conductivity (calc.)	uS/cm	386				
TDS (ion sum calc.)	mg/L	241				
SAR		0.20				
Langelier Index	S.I.	0.27				

Certified by Greg Clarkin, B.Sc., GeoChem Lab Manager

ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO, K2E 7T7 TELEPHONE: (613) 228 1145 FAX: (613) 228 1148

LABORATORY I.D.:	140192-2	CLIENTS JOB NUMBER:	Ian D. Wilson, #89-19
SAMPLE MATRIX:	Water, Bidan Subdivision	DATE SUBMITTED:	14-01-92
REPORT NUMBER:	7943001	DATE REPORTED:	30-01-92

METHOD: PURGE AND TRAP HIGH RESOLUTION GC-MS/SIM

PARAMETER	UNITS				
EPA 624		M.D.L.	Well 2		
Benzene	ppb	0.04	< 0.04		
Bromodichloromethane	ppb	0.09	< 0.09		
Bromoform	ppb	0.2	<0.2	 	
Bromomethane	ppb	0.4	<0.4	 	
Carbon Tetrachloride	ppb	0.08	< 0.08		
Chlorobenzene	ppb	0.05	< 0.05		
Chloroethane	ppb	0.4	<0.4		
Chloroform	ppb	0.06	< 0.06		
2-Chloroethylvinylether	ppb	0.09	< 0.09		
Chloromethane	ppb	0.6	< 0.6		
Dibromochloromethane	ppb	0.1	<0.1	 	
1,2-Dichlorobenzene	ppb	0.08	< 0.08		
1,3-Dichlorobenzene	ppb	0.07	< 0.07		
1,4-Dichlorobenzene	ppb	0.07	< 0.07		
1,1-Dichloroethane	ppb	0.1	<0.1		
1,2-Dichloroethane	ppb	0.1	<0.1		
1,1-Dichloroethene	ppb	0.2	< 0.2	 	
trans-1,2-Dichlorethene	ppb	0.1	<0.1		
1,2-Dichloropropane	ppb	0.2	< 0.2	 	
cis-1,3-Dichloropropene	ppb	0.1	<0.1		
trans-1,3-Dichloropropene	ppb	0.1	<0.1	 	
Ethylbenzene	ppb	0.03	< 0.03	 	
Methylene Chloride	ppb	0.05	< 0.05	 	
1,1,2,2-Tetrachloroethane	ppb	0.2	< 0.2		

ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO, K2E 7T7 TELEPHONE: (613) 228 1145 FAX: (613) 228 1148

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LABORATORY I.D.:	140192-2	CLIENTS JOB NUMBER:	Ian D. Wilson, #89-19
SAMPLE MATRIX:	Water, Bidan Subdivision	DATE SUBMITTED:	14-01-92
REPORT NUMBER:	7943001	DATE REPORTED:	30-01-92

METHOD: PURGE AND TRAP HIGH RESOLUTION GC-MS/SIM

PARAMETER	UNITS				
EPA 624		M.D.L.	Well 2		
Tetrachloroethene	ppb	0.08	< 0.08		
Toluene	ppb	0.04	<0.04	1	
1,1,1-Trichloroethane	ppb	0.08	< 0.08		
1,1,2-Trichloroethane	ppb	0.2	<0.2		
Trichloroethene	ppb	0.1	<0.1		
Trichlorofluoromethane	ppb	0.5	<0.5		
Vinyl Chloride	ppb	0.7	<0.7		
m,p-Xylene	ppb	0.03	< 0.03		
o-Xylene	ppb	0.03	< 0.03		

Certified by Greg Clarkin, B.Sc. GeoChem Lab Manager



Drinking Water System Number: 220007481 Drinking Water System Category: Small Municipal Residential Owned and Operated by: The Corporation of the Township of Tiny Report cov January 1st to December 31st, 2019

1. Notification and Availability of Reports:

The annual reports and annual summary reports are available to the public at no charge on the Township of Tiny website:

www.Tiny.ca

The Summary Report required under O. Reg. 170/03 Schedule 22 will be available for inspection at the Township of Tiny Municipal Office:

130 Balm Beach Rd W, Tiny, Ontario LOL 2J0

System users were notified that annual reports are available, free of charge, through the Township of Tiny website and when the public requests a report.

This Drinking Water System does not serve more than 10,000 people.

There are no Designated Facilities served by this Drinking Water System. A copy of this annual report was not provided to the Designated Facility but is available upon request.

The Township of Tiny does not report to any Interested Authorities.

There are no other Drinking Water Systems that receive all of their drinking water from this system.

2. Drinking Water System Description:

The Whippoorwill Drinking Water System is comprised of one pumping station, two groundwater wells, one storage reservoir, and approximately 2.6 km of distribution watermains. The system serves 71 properties, with 2 vacant lots slated for future service.



3. Water treatment chemicals used in this reporting period:

Sodium Hypchlorite (Flochem-12)

4. Significant expenses were incurred to:

- a. [x] Install required equipment
- b. [] Repair required equipment
- c. [x] Replace required equipment
- d. [] Studies / Engineering

5. Description and breakdown of monetary expenses incurred:

Total Expenditure:	\$107,349.00
Replaced reseroir probe	750.00
Cleaned generator fuel	850.00
Replaced all pumpstaion piping with stainless steel PH 21	105749.00

6. Details on the notices submitted in accordance with subsection 18(1) of the Safe Drinking-Water Act or section 16-4 of Schedule 16 of O.Reg.170/03 and reported to Spills Action Centre:

Incident Date	Parameter	Result	Unit of Measure	Corrective Action	Corrective Action Date
None					

7. Microbiological testing done under the Schedule 10, 11 or 12 of Regulation 170/03, during this reporting period:

Sample Locations	Number of Samples	Range of E. Coli results	Range of Total Coliform Results	Number of HPC Samples	Range of HPC Results
Raw	104	0	0-1	n/a	n/a
Treated	52	0	0	n/a	n/a
Distribution	52	0	0	52	0-210



8. Operational testing done under Schedule 7, 8 or 9 of Regulation 170/03 during the period covered by this Annual Report:

Parameter	Number of Grab	Range of	Results	
Parameter	Samples	(min #)-)-(max #)	
Turbidity - Raw	24	0.06	0.66	
Chlorine – Treated	228	1.15	2.14	
Chlorine - Distribution	105	0.78	1.87	
Fluoride – not required	n/a	n/a	n/a	

9. Summary of additional testing and sampling carried out in accordance with the requirement of an approval, order or other legal instrument:

Date of legal instrument issued	Parameter	Date Sampled	Result	Unit of Measure
None				

10. Summary of inorganic parameters tested during this reporting period or the most recent sample results:

Parameter	Sample Date	Results 21	Unit of Measure	Exceedance
Alkalinity	2019	164-175*	mg/L	no
Antimony	24-Apr-08	ND	μm	no
Arsenic	24-Apr-08	ND	μm	no
Barium	24-Apr-08	79	μm	no
Boron	24-Apr-08	14	μm	no
Cadmium	24-Apr-08	ND	μm	no
Chromium	24-Apr-08	ND	μm	no
Mercury	24-Apr-08	ND	μm	no
Selenium	24-Apr-08	ND	μm	no
Uranium	24-Apr-08	0.84	μm	no
Flouride	24-Apr-08	0.11	mg/L	no
Sodium	24-Apr-08	9400	μm	no
Lead	2018	ND-0.61*	μm	no
Nitrite	2019	<0.1	mg/L	no
Nitrate	2019	0.2-0.7	mg/L	no

Note: ND = not detected

*Distribution sample



11. Summary of organic parameters tested during this reporting period or the most recent sample results:

Parameter	Sample	Results	Unit	Exceedence
	Date	PH 21		
Alachlor	24-Apr-08	ND	μm	no
Atrazine + metabolites	24-Apr-08	ND	μm	no
Azinphos-methyl	24-Apr-08	ND	μm	no
Benzene	24-Apr-08	ND	μm	no
Benzo(a)pyrene	24-Apr-08	ND	μm	no
Bromoxynil	24-Apr-08	ND	μm	no
Carbaryl	24-Apr-08	ND	μm	no
Carbofuran	24-Apr-08	ND	μm	no
Carbon Tetrachloride	24-Apr-08	ND	μm	no
Chlorpyrifos	24-Apr-08	ND	μm	no
Diazinon	24-Apr-08	ND	μm	no
Dicamba	24-Apr-08	ND	μm	no
1,2-Dichlorobenzene	24-Apr-08	ND	μm	no
1,4-Dichlorobenzene	24-Apr-08	ND	μm	no
1,2-dichloroethane	24-Apr-08	ND	μm	no
1,1-Dichloroethylene (vinylidene chloride)	24-Apr-08	ND	μm	no
Dichloromethane	24-Apr-08	ND	μm	no
2,4-Dichlorophenol	24-Apr-08	ND	μm	no
2,4-Dichlorophenoxy acetic acid (2,4-D)	24-Apr-08	ND	μm	no
Diclofop-methyl	24-Apr-08	ND	μm	no
Dimethoate	24-Apr-08	ND	μm	no
Diquat	24-Apr-08	ND -	μm	no
Diuron	24-Apr-08	ND	μm	no
Glyphosate	24-Apr-08	ND	μm	no
Malathion	24-Apr-08	ND	μm	no
Metolachlor	24-Apr-08	ND	μm	no
Metribuzin	24-Apr-08	ND	μm	no
Monochlorobenzene	24-Apr-08	ND	μm	no
Paraquat	24-Apr-08	ND	μm	no
Pentachlorophenol	24-Apr-08	ND	μm	no
Phorate	24-Apr-08	ND	μm	no
Picloram	24-Apr-08	ND	μm	no
Polychlorinated Biphenyls (PCB)	24-Apr-08	ND	μm	no

Note: ND = not detected



Note:	ND	= nc	ot de	tected
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	Parameter	Sample Date	Results PH 21	Unit	Exceedence
Terbufos24-Apr-08NDμmnoTetrachloroethylene (perchloroethylene)24-Apr-08NDμmno2,3,4,6-Tetrachlorophenol24-Apr-08NDμmnoTriallate24-Apr-08NDμmnoTrichloroethylene24-Apr-08NDμmnoTrichloroethylene24-Apr-08NDμmnoTrichloroethylene24-Apr-08NDμmnoTrichlorophenol24-Apr-08NDμmnoTrichlorophenol24-Apr-08NDμmnoTrifluralin24-Apr-08NDμmno	Prometryne	24-Apr-08	ND	μm	no
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Trichloroethylene 24-Apr-08 ND μm no 2,4,6-Trichlorophenol 24-Apr-08 ND μm no Trifluralin 24-Apr-08 ND μm no	2,3,4,6-Tetrachlorophenol	24-Apr-08	ND	μm	no
2,4,6-Trichlorophenol 24-Apr-08 ND μm no Trifluralin 24-Apr-08 ND μm no	Triallate	24-Apr-08	ND	μm	no
Trifluralin 24-Apr-08 ND μm no	Trichloroethylene	24-Apr-08	ND	μm	no
	2,4,6-Trichlorophenol	24-Apr-08	ND	μm	no
Vinyl Chloride 24-Apr-08 ND µm no	Trifluralin	24-Apr-08	ND	μm	no
	Vinyl Chloride	24-Apr-08	ND	μm	no

Distribution Parameter	RAA	Exceedance
Haloacetic Acids Average	5.3	no
Trihalomethanes Average	6.3	no

12. The following inorganic or organic parameter(s) exceeded half the standard prescribed in Schedule 2 of Ontario Drinking Water Quality Standards:

Parameter	Result Value	Unit of Measure	Date of Sample
None			

Ontario,ca
records
Well

Ontario 😵 12/4/2020

31D/1240.B.

5706259

Mup: Well records

This map allows you to scurch and view well record information from reported wells in Onlario. Full dataset is available in the <u>Open Data catalogue</u>

Go Buck to Map

Well ID

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Midland Pumping Test

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WATER WELL RECORD

The Ortario Water Resources Commission Act

JTH [112]2 [57912] A 010 COSE

Lot 111 PRW Dite Completed 021

Well ID Number: 5706261 Well Audit Number: Well Tag Number:

riginal well record and any subsequent updates. This table contains information

Well Location

TINY TOWNSHIP 111 PR W 02 SIMCOE NO Concession Consty/District/Munichally Clty/Tewn/Village Address of Well Location Township Province Postal Code

NAD83 - Zone 17 Easting: 582814 30 Nurthing: 4954724.00 Municipal Plan and Sublet Number Other UTM Coordinates

Overburden and Bedrock Materials Interval

Central Calary Mart Common Marchall Other Marchals General Developed to Taylor Strong Strong

Annular Space/Abandonment Sealing Record

Depth Depth Type of Sealant Used Volume From To (Materiol and Type) Placed

Method of Construction & Well Use

Method of Constraction Well Use Cable Tool

Domestic

Status of Well

Construction Record - Casing Water Supply

Inside Open Hole or material Pepth Depth Diameter Open Hole or material From To 6 inch STEEL.

Construction Record - Screen

Outside Material Depth Depth Diameter Material From To 6 Inch 194 ft

Well Contractor and Well Technician Information

Pungking Nate 10 GPM Pungking Nate 24 NO m Flaal water beed 21 J R ff floring give rite 13 R Recommended pump depth 183 R

07116 12

Well Contractor's Licence Number: 4816

Results of Well Yield Testing

After test of well yield, water was CLEAR If pumping discontauce, give reason Pump intake set at

10 GPM 24 h:0 m

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https://www.ontario.ca/environment-and-energy/map-well-records

		Sandana a		
Inside diameter of casing 6 14 "	Static level 1.95	1954	4.	
Total length of casing 2.12 L.	Test-pumping rate	N		G.P.M.
Type of screen 6 " atom had steel	Pumping level 196	196	ŗł.	
Length of screen 3' x 25 alot 3. 2. x 30. alot	Duration of test pumping.	umping .	24 hou	
Depth to top of screen 2.13	Water clear or cloudy at end of test and	udy at end of 1	test clea	2
Diameter of finished hole	Recommended pumping rate	umping rate	0/	G.P.M.
	with pump setting of 203	5 of 20.		feet below ground surface
Well Log			Water	Water Record
Overburden and Bedrock Record	From ft.	ς. Έ	Depth(s) at which water(s) found	Kind of water (fresh, salty, sulphur)
sand gravel & stores	0	220	215	freak
For what purpose (a) is the water to be used? dome at is		Location of Well	of Well	
	In diagram road and	a below show lot line. Indi	In diagram below show distances of well from road and lot line. Indicate north by arrow.	l from arrow.
Is well on upland, in valley, or on hillside? Uparton of Drilling or Boning Firm	(F)	•	Le	Lotuz
Adires Craighart				
Licence Number 3481	<i>]</i>			11110,
Name of Driller or Borer R. Sinder				
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Map: Well records | Ontario.ca

Druw Down Time(min) Druw Down Water level Recovery Time(min) Recovery Water level SVL 160 R

10 GPM

12/4/2020 Recommended pump rute Weil Production Disinfected?

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Map: Well records | Ontario.ca

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Map: Well records

Ontario 😵

12/4/2020

This map allows you to search and view well record information from reported wells in Ontario. Full dataset is available in the Open Data catalogue.

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Well ID

Well ID Nunker: 727461 Well Tag Nunker: - 222034 Well Tag Nunker: - 222034 This table constart information from the original well record and any subsequent yadians:

Well Location

86 KING FISHER CRESCENT TINY TOWNSHIP 009 CON 12 SIMCUE PENETANG ON City/Town/Village Address of Well Location Township Province Postal Code Concession

NAD83 -- Zone 17 Easting: 581913.00 Northing: 4955590.00 Municipal Plan and Subjet Number Other UT'M Coordinates

Overburden and Bedrock Materials Interval

 Ceneral Colour
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 Description
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Annular Space/Abandonment Sealing Record

Depth Depth Type of Scalant Used Volume From To (Material and Type) Placed 0 ft 25 ft GROUT

Method of Construction & Well Use

Metiliod of Construction Well Use Other Method Domestic

Status of Well

Construction Record - Casing Water Supply

Construction Record - Screen

Outside Material Denth Denth Denth Diameter Material From To 5 inch STAINUJESS STFFEL 154 0 157 0.

Well Contractor and Well Technician Information

Results of Well Vield Testing Well Contractor's License Number, 2576

After test of well yield, water was CTEAR (pumping discontinued, give reason 100 fromp turies est at 110 ft Pumping Retter Duration of Pemping

ENVIRONMENT COPY

https://www.ontario.ca/environment-and-energy/map-well-records

Map: Well records | Ontario.ca

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Draw Down Time(anin). Draw Down Waler level. Recovery Time(anin). Recovery Water level SVL 96 ft Дгам Доңп & Recovery

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-	r)	ſ	4	5	10	15	92	25	30	40	45	50	99	
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	61		4	5	10	15	20	ž	30	01	45	Sn	60	

Water Details Water Found at Depth Kind 157 ft Fresh

Hole Dlameter Depth Depth Diameter From To Diameter ôft 20 ft Kinch 20 ft 337 ft 6 inch

Audit Number: 2227054 Date Well Cumpleted: Augest 90, 2016 Date Well Received by MOE: Jacuary 06, 2017 Updated: January 24, 2020

https://www.ontarlo.ca/environment-and-energy/map-well-records

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APPENDIX D

Test Pit Investigation (by Terraprobe)



December 3, 2020

File No. 3-20-0134-21 Barrie Office

Charlebois Properties Inc. 430 Concession 16 East Tiny, ON L9M 0P1

Attention: Mr. Frank Charlebois, frankc@charleboishaulage.com

RE: TEST PIT INVESTIGATION OVERHEAD BRIDGE ROAD TINY, ONTARIO

Dear Mr. Charlebois:

This letter presents the results of our Test Pit Investigation carried out at the above noted site. The purpose of the investigation was to retrieve samples for the estimation of soil percolation rates.

1. SITE AND PROJECT DESCRIPTION

The site is located at Overhead Bridge Road and the 12th Concession in the Township of Tiny, in the County of Simcoe, Ontario. The site consists of six lots, numbered one through six.

2. FIELD WORK

The field work for the investigation was carried out on November 24, 2020. The test hole locations are noted on the appended Test Pit Location Plan.

A total of six (6) test holes were advanced using an excavator extending to depths between 1.44 and of 1.8 m below existing grades.

The field work was carried out by a member of our field staff. The excavator was provided and operated by the client.

Greater Toronto 11 Indell Lane Brampton, Ontario L6T 3Y3 (905) 796-2650 Fax: 796TerroprobeInc.Hamilton – NiagaraCentral903 Barton Street, Unit 22220 BayStoney Creek, ON, L8E 5P5Barrie,(905) 643-7560 Fax: 643-(705) 73

Central Ontario 220 Bayview Drive, Unit 25 Barrie, Ontario L4N 4Y8 (705) 739-8355 Fax: 739-

Northern Ontario

1012 Kelly Lake Rd., Unit 1 Sudbury, Ontario P3E 5P4 (705) 670-0460 Fax: 670-

terraprobe ca

3. SUBSURFACE CONDITIONS

The details of the subsurface conditions encountered at the test pit locations are presented on the Table 1 summarized below. It should be noted that the conditions are confirmed at the test pit locations only and could vary between and beyond the locations. No water ingress was observed in all six test locations on the completion of excavation.

Lab No.	Location of sample	Soil Description	Unified Soil Classification	Estimated Soil "T"-Time (min/cm)	Depth of Test Hole (m)
719a	Lot 1	Sand, trace gravel, trace silt	SW-SP	4 to 6	1.44 m
719b	Lot 2	Sand, trace silt	SW-SP	4 to 6	1.8 m
719c	Lot 3	Sand, trace gravel, trace silt	SW-SP	4 to 6	1.5 m
719d	Lot 4	Sand, trace silt	SW-SP	4 to 6	1.6 m
719e	Lot 5	Sand, trace silt	SW-SP	4 to 6	1.8 m
71 9 f	Lot 6	Sand, trace silt, trace gravel	SW-SP	4 to 6	1.8 m

Table 1

Terraprobe witnessed the excavation of the test holes. Samples were retrieved between 0.5 and 1.2 m in the open test holes. Please refer to the appended Test Pit Location Plan. Terraprobe Inc. assumes no responsibility for the application of the above-noted percolation rates ("T"-Time) for use in design of an on-site sewage disposal system. The design of an on-site sewage system must be conducted by a qualified professional with due regard for a number of site-specific conditions in addition to the percolation rates of the soils.

4. ESTIMATTION OF SOIL PERCOLATION RATE ('T-TIME')

Samples were obtained of the native materials encountered in each of the six test holes. A grain size distribution curve was plotted for the samples and is appended on the Wash Sieve Analysis Test Reports. The estimated soil percolation rate ("T-Time") is greater than 4 to 6 min/cm.

5. CLOSURE

Terraprobe Inc. does not present the estimated percolation rates given in this report as a warranty of performance for the soils tested. Furthermore, the estimate provided is indicative of the sample in a disturbed state only. It must be emphasized that factors such as, but not limited to, consistency, structure, organic content, density and degree of saturation could influence the estimate. The client or third party using this information as a basis for tile field design assumes all risk associated with their evaluation of this report and all other criteria used in the design of any private sewage disposal system.

This report was prepared for the express use of Charlebois Properties and its retained design consultants and is not for the use by others. Contractors bidding on this project should provide their own interpretation of the data and/or conduct their own investigation and compose their own analyses/conclusions. This report is the copyright of Terraprobe Inc. and no part of this report may be reproduced by any means, in any form, without the prior written permission of Terraprobe Inc.

We trust this information is sufficient for your present purposes. Should you have any questions concerning the above, please do not hesitate to contact the undersigned.

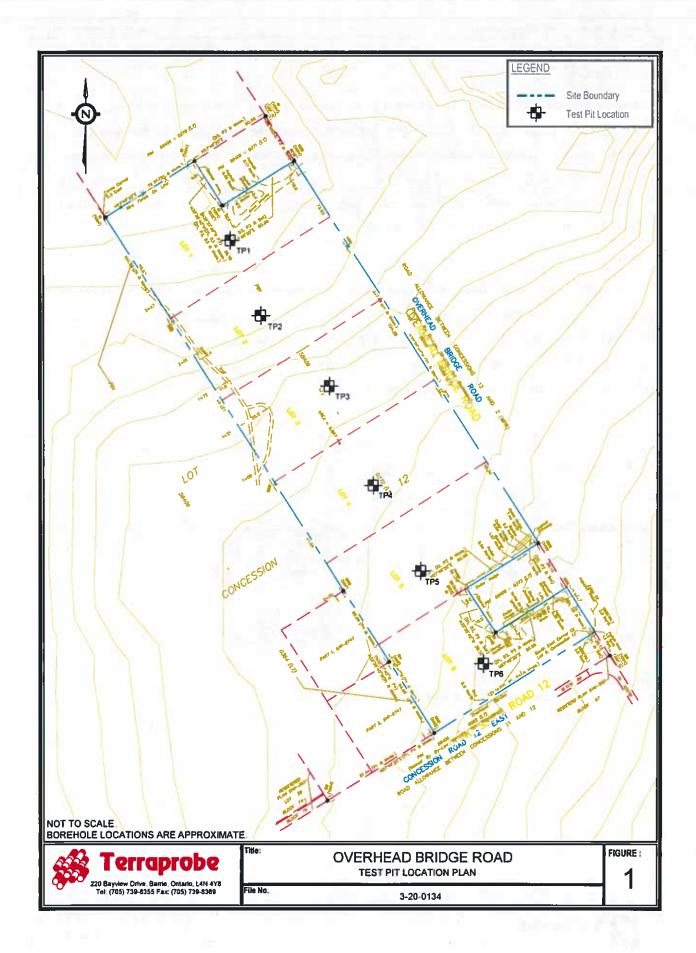
Terraprobe Inc. Steven Green, P.Eng

Associate Barrie Branch Manager

Enclosures: Test Pit Location Plan (1 page) Wash Sieve Analysis (6 pages)







Charlebois Properties Inc.

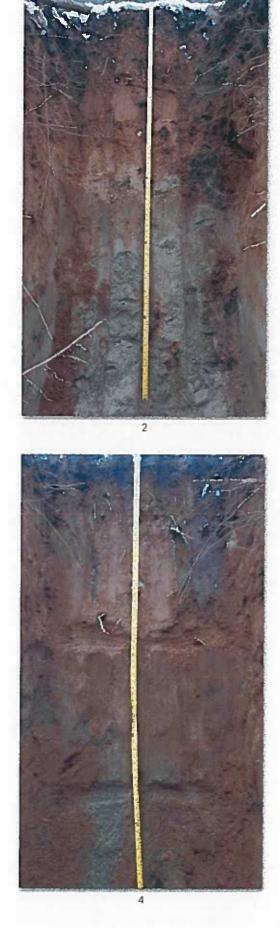
Overhead Bridge Road

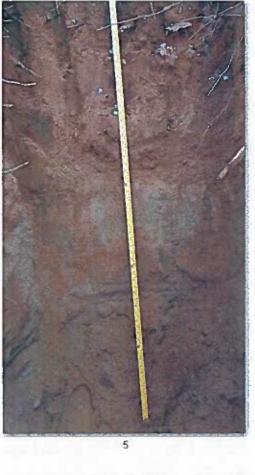
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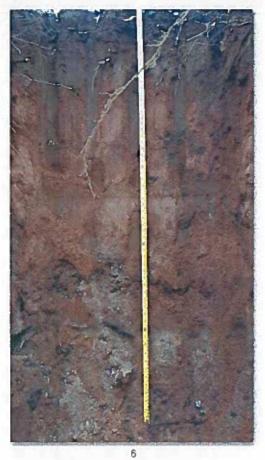


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Terraprobe

PROJECT: Overhead Bridge Road LOCATION: Tiny, ON CLIENT: Charlesbols Properties Inc.

TEST PIT NUMBER: 1 SAMPLE DEPTH: 0.5 to 1.5m

TEST REPORT

WASH SIEVE ANALYSIS

FILE NO.: 3-20-0134 LAB NO.: 719a SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

SAMPLE NUMBER: 1

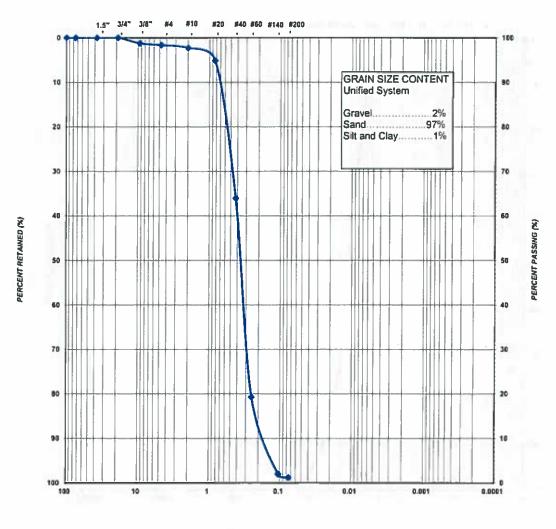
SAMPLE LOCATION: Lot 1

SAMPLE DESCRIPTION: Sand, trace gravel, trace silt

Estimated Septic T-Time: 4 to 6 mln/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



MIT	MIT		COARSE	MEDIUM	FINE				
MIT SYSTEM	GRAVEL		SAND			SILT	CLAY		
UNIFIED	COARSE	FINE	COARSE	MEDIUM	1	FRE			
SYSTEM				SAND			SILT AND CLAY		



WASH	SIEVE	ANAL	YSIS.
	TES	T REF	PORT

PROJECT: Overhead Bridge Road LOCATION: Tiny, ON CLIENT: Charlesbols Properties inc.

FILE NO.: 3-20-0134 LAB NO.: 719b SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

TEST PIT NUMBER: 2 SAMPLE NUMBER: 1

SAMPLE LOCATION: Lot 2

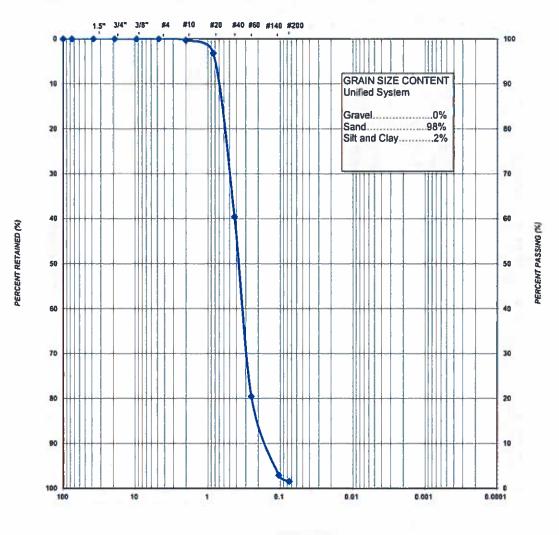
SAMPLE DESCRIPTION: Sand, trace slit

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

SAMPLE DEPTH: 0.5 to 1.5m

U.S. STANDARD SIEVE SIZES



MIT	NIT GRAVEL			COARSE	MEDIUM	FINE			
SYSTEM				SAND			SILT	CLAY	
	COARSE	FINE C	COARSE	MEDIUM		INE			
SYSTEM	SYSTEM GRAVEL			SAN	1D		SILT AND CLAY		



Тептаргове

PROJECT: Overhead Bridge Road LOCATION: Tiny, ON CLIENT: Charlesbols Properties Inc.

SAMPLE DEPTH: 0.5 to 1.5m

WASH SIEVE ANALYSIS TEST REPORT

FILE NO.: 3-20-0134 LAB NO.: 719c SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

TEST PIT NUMBER: 3

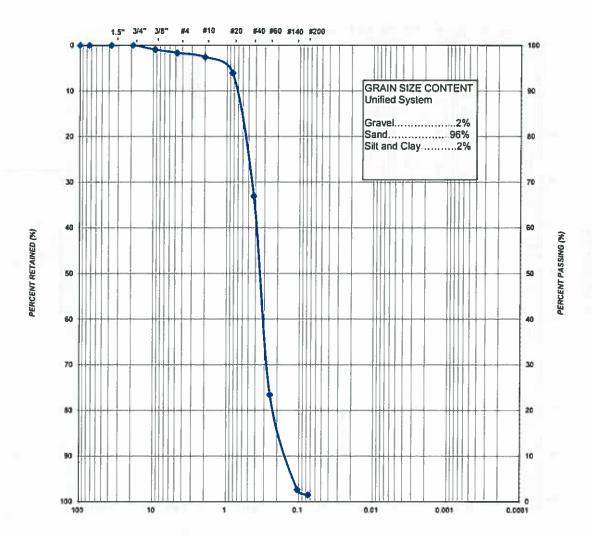
SAMPLE NUMBER: 1 SAMPLE LOCATION: Lot 3

SAMPLE DESCRIPTION: Sand, trace gravel, trace slit

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



MIT			L	COARSE	MEDIUM	FINE		
SYSTEM GRAVE		VEL			SAND		SILT	CLAY
UNIFIED	COARSE	FINE	COARSE	MEDIUM		FINE		
SYSTEM	GRAVEL			SAND			SILT AND CLAY	



PROJECT: Overhead Bridge Road

LOCATION: Tiny, ON CLIENT: Charlesbois Properties Inc.

TEST PIT NUMBER: 4

SAMPLE NUMBER: 1

SAMPLE LOCATION: Lot 4

SAMPLE DESCRIPTION: Sand, trace slit

WASH SIEVE ANALYSIS TEST REPORT

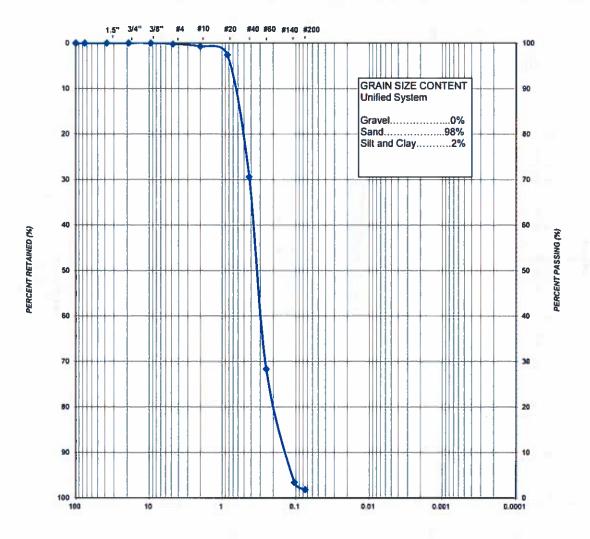
FILE NO.: 3-20-0134 LAB NO.: 719d SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

SAMPLE DEPTH: 0.5 to 1.5m

U.S. STANDARD SIEVE SIZES



MIT	- 1	COARSE	MEDIUM	FINE				
SYSTEM			SAND			SILT	CLAY	
UNIFIED	COARSE	FINE	COARSE	NEDIUM		FINE		
SYSTEM	GRAVEL			SAND			SILT AND CLAY	



Terraprobe

PROJECT: Overhead Bridge Road LOCATION: Tiny, ON CLIENT: Charlesbois Properties Inc.

SAMPLE DEPTH: 0.5 to 1.5m

TEST REPORT FILE NO.: 3-20-0134

WASH SIEVE ANALYSIS

LAB NO.: 719e SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

TEST PIT NUMBER: 5

SAMPLE NUMBER: 1 SAMPLE LOCATION: Lot 5

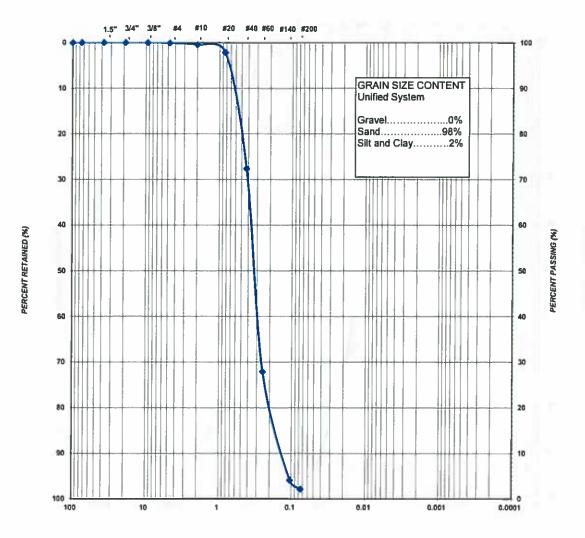
CAMPLE DESCRIPTION: Cord Arrow

SAMPLE DESCRIPTION: Sand, trace slit

Estimated Septic T-Time: 4 to 6 mln/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



MIT SYSTEM	GR/	GRAVEL			MEDIUM SAND	FINE	SILT	CLAY
UNIFIED	COARSE	FINE	COARSE	MEDIUM		FINE		
SYSTEM	GRAVEL			SAND			SILT AND CLAY	



PROJECT: Overhead Bridge Road	
LOCATION: Tiny, ON	
CLIENT: Charlesbois Properties	inc

SAMPLE DEPTH: 0.5 to 1.5m

TEST PIT NUMBER: 6 SAMPLE NUMBER: 1

SAMPLE LOCATION: Lot 6

SAMPLE DESCRIPTION: Sand, trace slit, trace gravel

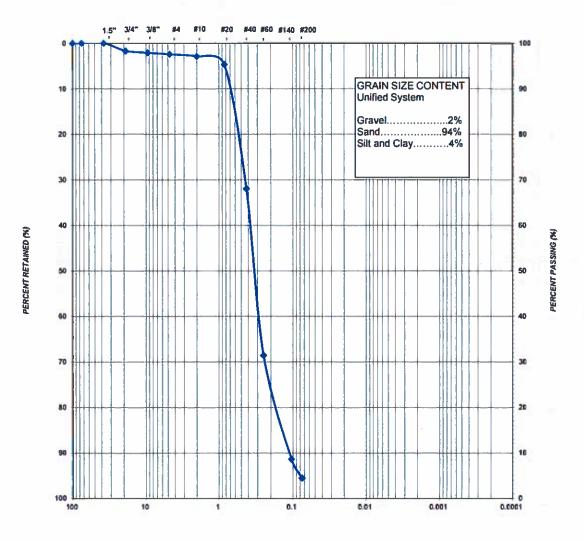
WASH SIEVE ANALYSIS **TEST REPORT**

FILE NO.: 3-20-0134 LAB NO .: 719f SAMPLE DATE: Nov-24-20 SAMPLED BY: S.W.

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



MIT	MIT		COARSE	MEDIUM	FINE				
MIT SYSTEM	GRAVEL		SAND			SILT	CLAY		
UNIFIED	COARSE	FINE	COARSE	MEDIUM	_	FINE			
SYSTEM	STEM GRAVEL			SAI	dir.	-	SILT AND CLAY		

APPENDIX E

Traffic Calculations



WMI & Associates Limited 119 Collier Street, Barrie, Ontario L4M 1H5 p (705) 797-2027 f (705) 797-2028

TRIP GENERATION SPREADSHEET

VEHICLE TRIP ENDS VS. DWELLING UNITS ON A WEEKDAY, PEAK HOUR OF ADJACENT STREET TRAFFIC, ONE HOUR BETWEEN 7AM AND 9AM

Date: 1-Dec-20

Project No.: 20-644

Project: Charlebois Properties, Tiny Twp.

Prepared By: JR

References: Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th edition

Development	ITE Code & Land Use	Independent Variable	Total Trips- From Fitted Curve Equation [T = 0.71(X) + 4.80]
Charlebois Properties	210: Single-Family Detached Housing	6 units	10

Notes:

This analysis is based on the Concept Plan for NW corner of Overhead Bridge Rd. & Concession 12 E, prepared by Celeste Phillips Planning Inc., dated November 6, 2020.

\\WMI-SERVER\wmi-server\Data\Projects\General Project Info\[Master Project List.xlsx]MASTER



WMI & Associates Limited 119 Collier Street, Barrie, Ontario L4M 1H5 p (705) 797-2027 f (705) 797-2028

TRIP GENERATION SPREADSHEET

VEHICLE TRIP ENDS VS. DWELLING UNITS ON A WEEKDAY, PEAK HOUR OF ADJACENT STREET TRAFFIC, ONE HOUR BETWEEN 4PM AND 6PM

Date: 1-Dec-20

Project No.: 20-644

Project: Charlebois Properties, Tiny Twp.

Prepared By: JR

References: Institute of Transportation Engineers (ITE) Trip Generation Manual, 10th edition

Development	ITE Code & Land Use	Independent Variable	Total Trips- From Fitted Curve Equation [Ln(T) = 0.96Ln(X) + 0.20]
Innisfil Executive Estates Phase 2	210: Single-Family Detached Housing	6 units	7

Notes:

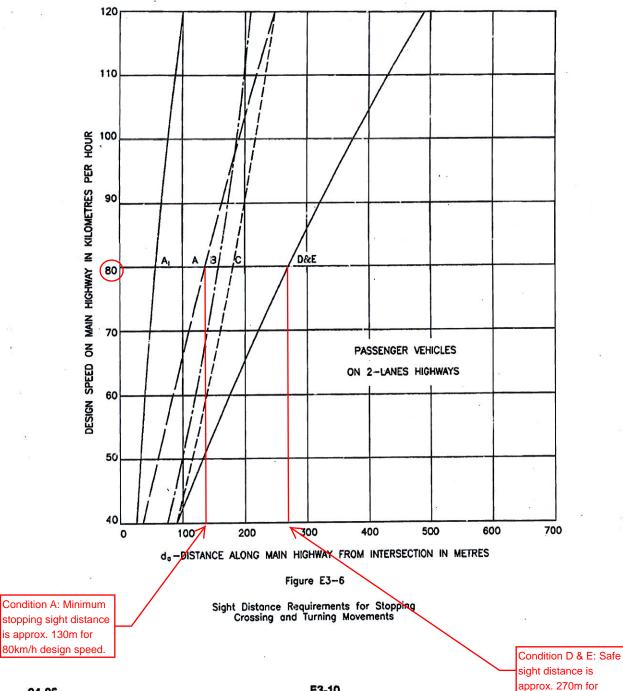
This analysis is based on the Concept Plan for NW corner of Overhead Bridge Rd. & Concession 12 E, prepared by Celeste Phillips Planning Inc., dated November 6, 2020.

\\WMI-SERVER\wmi-server\Data\Projects\General Project Info\[Master Project List.xlsx]MASTER

AT-GRADE INTERSECTIONS

80km/h design speed.

- A Minimum Stopping Sight Distance, Table E3-1.
- A1 Distance travelled in 3 s, Table E3-2.
- B Safe Sight Distance for P vehicle, crossing 2-lane highway from stop.
 C Safe Sight Distance for P vehicle, turning left into 2-lane highway across P vehicle approaching from left.
- D Safe Sight Distance for P vehicle to turn left into 2-lane highway and attain assumed operating speed before being overtaken by P vehicle approaching in same direction at design speed.
- Ε-Safe Sight Distance for P vehicle to turn right into 2-lane highway and attain assumed operating speed before being overtaken by P vehicle approaching in same direction at design speed.



94-06

APPENDIX F

Project Correspondence

Stephen Morash

From: Sent: To: Cc: Subject: Celeste Phillips <celeste@cplan.ca> November 30, 2020 4:30 PM Stephen Morash Frank Charlebois FW: Charlebois development

Stephen – Below is the email exchange with Melissa. Sounds good to me – but please let us know.

From: "celeste@cplan.ca" <celeste@cplan.ca>
Date: Monday, November 30, 2020 at 4:27 PM
To: Melissa Carruthers <MCarruthers@severnsound.ca>
Cc: Shawn Persaud <spersaud@tiny.ca>
Subject: Re: Charlebois development

Thanks Melissa for your response. Yes, 6 residential lots are contemplated, no commercial or retail.

From: Melissa Carruthers <MCarruthers@severnsound.ca>
Date: Monday, November 30, 2020 at 10:04 AM
To: "celeste@cplan.ca" <celeste@cplan.ca>
Cc: Shawn Persaud <spersaud@tiny.ca>
Subject: RE: Charlebois development

Hi Celeste,

I can only speak to the drinking water source protection program and the screening that I do as part of that on behalf of the Township; as this property is located in the wellhead protection area D of the Robert Street municipal drinking water system, with a vulnerability score of 2. If the application is strictly for the creation of 6 residential lots, without any commercial or retail spaces, I would not have any requirements. Having said that, once a formal application has been made, I would issue a letter to this effect. In essence, formal screening will take place, however, based on the indicated plans for the property, nothing will apply from a drinking water source protection standpoint.

For all other screening requirements, it's recommended to confirm with Shawn and Calvin.

If you have any questions, comments, or concerns, please feel free to contact me. Thank you!

Melissa Carruthers Risk Management Official / Risk Management Inspector

Severn Sound Environmental Association 489 Finlayson St, P.O. Box 460, Port McNicoll, ON L0K 1R0 P (705) 534-7283 ext. 205 / Fax (705) 534-7459 MCarruthers@severnsound.ca | www.severnsound.ca | @SSEA_SSRAP

** OFFICE CLOSED**

As the circumstances caused by COVID-19 continue to evolve, the SSEA office remains closed. The SSEA staff will continue to operate remotely. We expect this to cause delays in our ability to respond to requests. For more information see <u>www.severnsound.ca</u>

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From: Celeste Phillips [mailto:celeste@cplan.ca] Sent: November 25, 2020 5:33 PM To: Melissa Carruthers Subject: Charlebois development

Hi Melissa – We recently met at a virtual meeting regarding the Charlebois landholding on the west side of Overhead Bridge Road in the Township of Tiny. My recollection is that Shawn Persaud indicated at the outset of the meeting that no formal screening is required and I was wondering if you might have provided this to Shawn by email. He is away this week and I wanted to be sure I had your confirmation of this. Kindly advise when time permits.

Celeste Phillips, MCIP RPP

Celeste Phillips Planning Inc.

85 Bayfield Street Suite 300 Barrie, Ontario Canada L4M 3A7

Telephone: 705.797.8977 iPhone: 705.730.8850

Email: celeste@cplan.ca

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